Synergetic Effects of Graphene and Nonfunctionalized Carbon Nanotubes Hybrid Reinforced Epoxy Matrix on Mechanical, Thermal and Wettability Properties of Nanocomposites

Ahmed A. Moosa^{1,*}, Ahmad Ramazani S. A.², Faris Abdul Karim Kubba³, Maysam Raad¹

¹Department of Materials Engineering Technology, Engineering Technical College, Middle Technical University Baghdad, Iraq ²Department of Chemical and Petroleum Engineering, Sharif University of Technology, Tehran, Iran ³Engineering Technical College, Middle Technical University Baghdad, Iraq

Abstract In this study we focused on the effect of Graphene Nanoplates (GNPs) and Nonfunctionalized Multi Wall Carbon Nanotubes (MWCNTs) hybrid nanofiller and its dispersion on mechanical, wettability, and thermal stability properties of epoxy nanocomposites. The epoxy resin was mixed with 0.5wt. % (GNPs-MWNTs) by direct mixing method using different (GNPs:MWNTs) ratio as (0:10, 1:9, 2.5:7.5, 5:5, 7.5:2.5, 9:1 and 10:0). The dispersionability of carbon nanofiller in epoxy nanocomposite samples was examined by FESEM. The results indicate that epoxy /GNPs significantly out-perform MWNTs additives. The superiority of GNPs in terms of mechanical properties improvement over MWNTs may be due to their high aspect ratio, improved nanofiller matrix adhesion/interlocking arising from their wrinkled surface, and their geometry (2D structure). The best improvements in mechanical properties was found at two mixing ratios of GNPs: MWNTs (5:5) and (9:1). The improved mechanical properties of epoxy/GNPs- MWNTs hybrid nanocomposite is related to the formation of 3-D hybrid architectures structure in epoxy matrix as confirmed by FESEM observations. The hydrophobicity of Epoxy/0.5 wt. % MWNTs is higher than that of epoxy/0.5wt.% GNPs, where contact angle of Epoxy/MWNTs is larger than that of epoxy/ 0.5wt. % GNPs and water absorption of Epoxy/ 0.5wt. % MWNTs is less than that for epoxy/ 0.5wt. % GNPs. Hydrophilicity of neat epoxy decreases by adding 0.5 wt.% GNPs-MWNTs with mixing ratio 2.5:7.5 where contact angles are changed from 43.5° to 79.5°. Thermogravimetric analysis results for neat epoxy, Epoxy/MWNTs, Epoxy/GNPs-MWNTs do not show any major influence on thermal stability of epoxy.

Keywords Hybrid nanocomposites, Multi-walled carbon nanotubes, Graphene, Epoxy, Tensile Strength

1. Introduction

The significant improvement of the properties of polymeric materials can be achieved by adding nanofillers. The properties of Polymer nanocomposites are significantly higher than properties of conventional composites. Where it has unique combination of electrical, mechanical and thermal properties [1]. These properties depending on the type and loading amounts of the fillers, matrix, the nanofiller dispersion and the type of bonding at matrix/nanofiller interface [2, 3]. Polymer nanocomposites have been used in various fields of engineering and science such as electronics, sensors, photovoltaic cell, coating and mechanical structures for a lot various applications such as automotive industries,

aerospace industries, medical equipment, defense systems.

Carbon nanotubs (CNTs) have been used as a prominent nanofiller material since their discovery in 1991 by Iijima [4]. Graphene nanoplates (GNPs) have attached the attention of many researchers since their discovery in 2004 by Navoselov [5] because of its unique properties.

GNP is a honeycomb lattice structure of sp2 hybridized carbon atoms arranged into a two-dimensional (2D) planar monolayer with a carbon–carbon bond length of 0.142 nm [1, 5]. CNTs are long-hollow cylinder structures formed by rolling single layer or multilayer's of graphene into one-dimensional (1D), which are honeycomb hexagonal lattice of the carbon's atoms have sp2 hybridization and capped by half – fullerenes [6, 7].

Carbon nanotubes (CNTs) and graphene nanoplates (GNPs) share many similar properties, but on the other hand differ in other aspects because of the structural differences. Attempts have recently been made to integrate these two carbon-based materials in order to utilize the merits of both

^{*} Corresponding author:

ahmeda1752@yahoo.com (Ahmed A. Moosa)

Published online at http://journal.sapub.org/materials

Copyright © 2017 Scientific & Academic Publishing. All Rights Reserved

[8]. Carbon nanotubes possess excellent electrical conductivity and they can be added to a poor electroconductive polymer and enhances its electrical properties [9]. Similarly, graphite nanoplatelets (GNPs) possess excellent thermal conductivity of $3000 \text{ Wm}^{-1}\text{K}^{-1}$ and they can successfully improve the thermal conductivity of polymer [10].

Graphene exhibits extraordinary properties. These properties emerge only in the 2D planar direction of the graphene structure, limiting its scope and applications. This weakness was overcome by adding (1-D) MWCNTs to (2-D) GNPs to form 3D structures. In these (3-D) hybrid architectures, these arms entangle with polymer chain to provide stronger interaction between MWCNTs/ GNPs and the epoxy matrix which Minimizing the aggregation of GNPs [11]. Thus, the combining (1-D) MWCNTs and (2-D) GNPs will become very important concepts for improving the performance of graphene-based polymer nanocomposites and may be a solution to an ever increasing market demand for polymer nanocomposites with balanced mechanical properties. The advantage of polymer nanocomposite is to provide newly added good properties to the neat polymer without sacrificing its processability, light weight and inherent mechanical properties [12]. Several challenges need to be resolved in order to utilize the enhanced mechanical, electrical, thermal, optical, and chemical properties of nanocomposites. These challenges include: the development of better dispersion methods of nanofillers in polymeric matrices; to develop a proper techniques to control the interface and to reduce the cost [11]. The aim of this work is to study the effect of dispersion of GNPs with nonfunctionalize MultiWalls Carbon Nanotubes (MWNTs) as hybrid nanofillers on mechanical, wettability and thermal stability properties of polymer nanocomposite. The Epoxy/GNPs-MWNTs nanocomposites have fixed weight fraction of nanofillers and prepared under the same process conditions and parameters.

2. Experimental Work

2.1. Materials

Epoxy resin (Epikote 828) (density = 1.16 g/cm^3 , viscosity = 110-150 Poise) and aliphatic amines hardener (EPI-CURE curing agent 3234) produced from triethylenetetramine (TETA) were obtained to prepare epoxy nanocomposite samples. Graphene Nanoplates (GNPs), Grade C-750 with 97% purity consist of 4-5 graphene layers with an average diameter of 1 micron and an average thickness of 2 nm was purchased from XG Science Company, Lansing, MI, USA. Nonfunctionalized Multiwalled Carbon Nanotubes (MWCNTs) with 50 μ m in length and 8-15 nm in diameter were obtained from Neutrino Nanovation, TECNAN Company, China.

2.2. Preparation of Nanocomposites

The experimental work was done at (Nano-Technology Center Laboratory/ Institute for Nanotechnology and Nanoscience / Sharif University of Technology/ Tehran/ Iran). The epoxy/GNPs-MWNTs nanocomposites samples were prepared by direct mixing method as reported by Moosa et al., 2016) [13]. The epoxy resin was mixed with 0.5wt.% (GNPs+MWNTs) using different mixing ratio (0:10, 1:9, 2.5:7.5, 5:5, 7.5:2.5, 9:1 and 10:0) of (GNPs:MWNTs).

2.3. Characterization and Instruments

The tensile properties of epoxy nanocomposite samples were measured using Universal Testing Machine (HIWA 200, model 2125, HIWA Eng. Co., Korea) with loading rate 5 mm/min at room temperature. The fracture surfaces of epoxy/GNPs-MWNTs nanocomposites were examined by Field Emission Scanning Electron Microscope (FESEM) with spatial resolution down to 1.5 nm (Mira 3 Tescan FESEM, Czech).

The thermogravimetric (TG) analyzer TGA/DSC 1 (METLER TOLEDO Company, USA) was used under nitrogen gas atmosphere within the temperature range from room temperature to 700°C and heating rate of 10°C/min to evaluate the thermal stability of all the fabricated nanocomposite samples as a function of the temperature.

The wettability properties of fabricated nanocomposite samples were characterized by measuring the static contact angles of the liquid drop over the surface of the nanocomposite samples using optical microscope, and the water absorption through the epoxy nanocomposite samples.

3. Results and Discussion

3.1. Tensile Properties of Epoxy/GNPs-MWNTs Nanocomposites

The tensile strength mechanical properties of Epoxy/GNPs-MWNTs hybrid nanocomposites containing fixed weight fraction of GNPs:MWNTs hybrids (0.5wt%) with different mixing ratio (0:10, 1:9, 2.5:7.5, 5:5, 7.5:2.5, 9:1and 10:0) of GNPs:MWNTs are shown in Figure 1. The tensile strength increments are 27%, 46%, 50%, 53%, 52%, 60% and 59% at GNPs:MWNTs mixing ratios of 0:10, 1:9, 2.5:7.5, 5:5, 7.5:2.5, 9:1and 10:0 respectively.

The tensile strength with mixing ratio of (9:1) GNPs:MWNTs was higher than that for neat epoxy or single type of carbon nanomaterial reinforced epoxy (0:10 and 10:0). This is because of the flexible 1-D structure MWNTs with the 2-D structure GNPs can form 3-D hybrid architectures. These 3-D architectures will inhibit face to face aggregation of GNPs. Thus, the contact surface area between GNPs-MWNTs and epoxy matrix increased, and also MWNTs can act as extended coordinating arms for the 3D hybrid architectures, which can become entangled with

the polymer chain resulting better interaction between GNPs-MWNTs hybrid and the epoxy matrix [11, 14].

The Young's modulus shows 6%, 16%, 19%, 27%, 13%, 22% and 62% increments at 0:10, 1:9, 2.5:7.5, 5:5, 7.5:2.5, 9:1 and 10:0 GNPs:MWNTs mixing ratios, respectively as shown in Figure 2. At 7.5:2.5 GNPs:MWNTs the Young's modulus start decreasing but still higher than that of neat epoxy.

The results showed that GNPs significantly out-perform MWNTs addition. The Young's modulus of the epoxy/GNPs nanocomposite was 62% greater than the neat epoxy as compared to 6% increase for MWNTs.



Figure 1. Tensile strength of Epoxy/GNPs-MWNTs nanocomposites

The tensile strength of the neat epoxy was enhanced by 59% with GNPs compared to 27% improvement for MWNTs. The uniform dispersion of GNPs mainly contributes to the higher tensile modulus. In addition, the better synergetic effect between GNPs and MWNTs will improve the mechanical properties of the nanocomposites.



Figure 2. Young's modulus of Epoxy/GNPs-MWNTs nanocomposites

The lower improvement in the tensile modulus and strength in the epoxy nanocomposites may be attributed to the waviness of pristine MWNTs and nonuniform dispersion of the MWNTs arising from Van der Waals force and π - π interaction. This will led to the formation of aggregations which behave like micrometer size defect and act as stress concentration sites [11]. The lower mechanical properties of nanocomposite with GNPs-MWNTs mixing ratios 7.5:2.5 can be attributed to the formation of aggregated sheets of GNPs. Also the GNPs agglomerates would form steric

obstacles, restricting the flow of polymer into the agglomerates and resulting in the formation of holes and voids between GNPs and epoxy [11]. These results are compatible with the work of (Wang et al. 2015) [14] who prepared epoxy resin containing uniformly dispersed 1wt% CNTs/GNPs hybrids with different mixing ratio (i.e., 10:0, 9:1, 7:3, 5:5, 3:7, 1:9, and 0:10). The results showed that the tensile strength of nanocomposite is lower with GNPs/CNTs hybrids mixing ratios at 7:3.

The fracture strains decreases with addition of GNPs and it is lower than that of neat epoxy, but it is increase with the addition of MWNTs or GNPs-MWNTs hybrid and it is higher than that of neat epoxy, Figure 3. This means that the addition of GNPs to epoxy lead to increase the brittle behaviour of samples and the addition of MWNTs or GNPs-MWNTs hybrid to epoxy lead to decrease the brittle behaviour of samples. The percentage of increase in elongation shows 11%, 49%, 24%, 39%, 47%, 55% and - 39% increments at 0:10, 1:9, 2.5:7.5, 5:5, 7.5:2.5, 9:1 and 10:0 GNPs:MWNTs mixing ratios, respectively.



Figure 3. Elongation at ultimate tensile strength of Epoxy/GNPs-MWNTs nanocomposites

3.2. FESEM of Fracture Surface of Epoxy/GNPs-MWNTs Hybrid Nanocomposite

FESEM images of the neat epoxy, Figure 4 (a), shows smooth fracture surface and this means the crack through growth is not obstructed by any obstacles.

The FESEM images of Epoxy/GNPs nanocomposite show better dispersion than Epoxy/MWNTs as shown in Figure 4 (b) and Figure 4 (c) respectively. These samples contain fixed weight fraction of nanofillers (0.5 wt. %) and prepared in the same procedure. In the Epoxy/ GNP-MWNTs with mixing ratio 0:10, MWNTs tend to entangle due to Van der Walls attraction forces and π - π interaction between nanotubes. The agglomerates in Epoxy/MWNTs nanocomposite, Figure 4 (c) act as stress concentration sites, which are absence in epoxy/GNPs.

In MWNTs reinforced epoxy crack bridging mechanisms play important role in improved fracture toughness of nanocomposite samples. Large energy dissipated within bridging mechanisms due to very small diameter in nanoscale and large length in microscale of nanotubes and crack deviation may take secondary role [15]. When a nanotubes bridge two fracture surfaces, it may either fracture or pulled out from one of the surfaces and appear to lie on the fracture surface depending on the flexibility of the nanotubes,

epoxy-nanotubes interfacial strength (interfacial bonding), embedded length and angle to fracture surface of nanocomposite [16].



Figure 4(a). FESEM images of neat epoxy [Mag. 10 kx]



Figure 4(b). Epoxy/GNPs(0.5wt.%) [Mag. 18.0 kx]



Figure 4(c). Epoxy/MWNTs (0.5wt.%) [Mag.10.0kx]



Figure 4(d). Epoxy/GNPs-MWNTs [1:9] (0.5 wt.%) [Mag.7.00 kx]



Figure 4(e). Epoxy/GNPs-MWNTs hybrid [9:1] (0.5 wt.%) [Mag.42.0kx]



Figure 4(f). Epoxy/GNPs-MWNTs [7.5:2.5] (0.5 wt.%) [mag.12.2kx]



Figure 4(g). Epoxy/GNPs-MWNTs [5:5] (0.5 wt.%) [mag.107kx]



Figure 4(h). Epoxy/GNPs-MWNTs [1:9] (0.5 wt.%) [mag.154kx]

The degree of pulling indicates the weak interfacial bonding between epoxy- nanofiller. No GNPs appeared (no pullout) on fracture surface of Epoxy/ 0.5wt% GNPs and this indicates strong interface interaction, Figure 4(b). In Figure 4 (c), MWNTs appeared (pullout) to lie on the fracture surface and this indicates weak interface interaction between that MWNTs and the epoxy.

Figure 4 (d) shows GNPs:MWNTs nanocomposite with mixing ratio 1:9. The MWNTs tend to tangled and twisted with each other and stack on GNPs. Thus, high weight fraction of MWNTs (0.45 wt%) has lower chance to disperse between GNPs. A 3-D hybrid architectures is formed at GNPs:MWNTs mixing ratio of 9:1, as shown in Figure 4 (e). At low weight fraction of MWNTs (0.05 wt%) there is enough MWNTs to be dispersed between (0.45 wt%) GNPs.

For GNPs:MWNTs hybrid nanocomposite with mixing ratio 7.5:2.5, the agglomeration of nanofillers, Figure 4 (f). lower the mechanical properties of the nanocomposites.

FESEM image with high magnification for Epoxy/GNPs-MWNTs are shown in Figure 4 (g) and 4(h). Nonfunctionalized MWNTs have better chance to hybrid and bond with GNPs because there are no functional group which impede and reduce the bonding chance as reported by (Moosa et al., 2016) [13].

3.3. Thermogravimetric Analysis (TGA)

Residual weight percentage versus temperature curve is shown in Figure 5 where the thermal of the nanocomposite specimens are slightly different. The thermal stability analyses curves, Figure 5, of neat epoxy and its nanocomposite samples can be explain by dividing them into three steps: initial decomposition, Tg curve, and complete decomposition. At the initial very small decomposition appears over all samples, the same may be created by the loss of volatiles. We can evaluate the thermal stability of the neat epoxy and its nanocomposite samples by Td (the temperature at the 5% weight loss identified as the onset temperature of decomposition) and Tmax (the temperature at the 50% weight loss identified as the devastation temperature of composite structure).

Table 1. TGA analysis (T5%, and T50%) of neat epoxy and its nanocomposites

Sample	$T_{d}[^{\circ}C](a)$	$T_{max} [°C] (b)$
Neat Epoxy	348	393
Epoxy/MWNTs	345	395
Epoxy/GNPs	345	396
Epoxy/GNPs-MWNTs	345	400

(a) T_d : The degradation temperature at the 5% weight loss in the decomposition stage

(b) T_{max} . The degradation temperature at the 50% weight loss in the decomposition stage

We can obtain information for the thermal degradation behavior from these details as mention in Table 1. The devastation in composite structure (50% weight loss) occurred when exposed to heat at 396+4°C. Thus, GNPs and MWNTs nanofillers may be affected by the temperature because variation in weight loss at the third stage, where all specimens start variation after temperature 374°C, as shown in Figure 5.



Figure 5. TGA of neat epoxy and its nanocomposites

Clearly, from the results of the epoxy/GNPs, the addition of GNP to epoxy can increase the complete decomposing temperature (i.e increase thermal stability of epoxy at third stage and decreased weight loss percentage). At temperature 471°C the loss weight (73%, 70%, 72% and 75%) for each of (neat epoxy, Epoxy/GNPs, Epoxy/MWNTs and Epoxy/GNPs-MWNTs hybrid) respectively.

Decrease the weight loss percentage with temperature rise means improves interfacial interaction between epoxy matrix and the GNPs in nanocomposites [17]. Higher energy needed to overcome on the strong interfacial bonding between GNPs and epoxy in nanocomposite samples .And also the graphene nanoplate thermal conductivity is, 5000 $Wm^{-1}K^{-1}$ [18]. It was higher than the MWCNTs thermal conductivity is 3000 $Wm^{-1}K^{-1}$ [19]. This explains that graphene nanoplates can help to dissipate the heat more quickly in epoxy than MWNTs [20].

Also the decomposition temperatures were almost the same for all the nanocomposites $395\pm 5^{\circ}$ C. This is an indication that the heat destruction was not dependent on the content of nanofillers. These finding also supported by the work of (Mir and Kumar, 2012) [21], where they used (0.1%, 0.2%, 0.3% and 0.4%) MWNTs as nanofiller. They concluded from their results that MWNT incorporation does not have a significant effect on the thermal degradation of epoxy systems. (Le and Huang, 2015) [22] used GNPs to reinforce an epoxy/polyester blend. The TGA results confirmed the thermal stability of the resulting nanocomposite specimens, regardless of the weight percentage of the GNPs.

3.4. Differential Thermogravimetry (DTG)

Differential thermogravimetry (DTG) (first derivative) was used to evaluate the peak degradation temperature of (Neat epoxy, Epoxy/MWNTs, Epoxy/GNPs and Epoxy/GNPs-MWNTs hybrid) with loading amount

0.5 wt.% of nanofillers. Table 2 and Figure 6 show the degradation temperatures (T_{DTG}) of neat epoxy and its nanocomposite samples. The first degradation temperature (T_{DTG1}) for epoxy/GNPs and epoxy/ GNPs-MWNTs hybrid is (360°C) it was 10°C lower than T_{DTG1} of epoxy/MWNTs and 7°C lower than T_{DTG1} of neat epoxy. This may be related to good dispersion of GNPs and GNPs-MWNTs hybrid in epoxy. Where GNPs and GNPs-MWNTs hybrid act as barrier hinders the crosslink reaction between epoxy chains, consequently this will reduce the crosslink reaction.

Table 2. Degradation temperature of neat epoxy and its nanocomposites with loading amount 0.5 wt.% of nanofillers

Sample	T_{DTG1} [°C]	T_{DTG2} [°C]	$T_{DTG3}[^{o}C]$
Neat epoxy	367		549
Epoxy/GNPs	360		576
Epoxy/MWNTs	370		597-600
Epoxy/GNPs-MWNTs	360	374	573

3.5. Contact Angle of Epoxy/GNPs-MWNTs Nanocomposite

Figure 7 shows contact angle for Epoxy/GNPs-MWNTs hybrid nanocomposite samples with fixed nanofiller weight fraction (0.5 wt.%) and different mixing ratio (0:10, 1:9, 2.5:7.5, 5:5, 7.5:2.5, 9:1, 10:1). The neat epoxy (hydrophilic) has 43.5° as a contact angle. The contact angles of different ratios of GNPs: MWNTs are higher than that for neat epoxy. The range of contact angle for Epoxy/GNPs-MWNTs composite is between (44.5° - 79.5°) corresponding to GNPs:MWNTs ratio ranges 0:10 - 10:0. The maximum contact angle is 79.5° at GNPs:MWNTs ratio 2.5:7.5 and at this ratio the wettability of Epoxy/GNPs-MWNTs composite decreased. The poor water adhesion is caused by more uniform and compact MWNTs coverage on the graphene nanosheets.

Figure 7 indicates that the epoxy / GNPs is more hydrophilic than epoxy / MWNTs with the same weight fraction 0.5% of nanofiller.



Figure 6. DTG thermograms for neat epoxy and its nanocomposites



Figure 7. Contact angle for Epoxy/GNPs-MWNTs Nanocomposites

3.6. Water Absorption of Epoxy/GNP-MWNT Nanocomposite Samples

Figure 8 show the water absorption percentage of Epoxy/GNPs-MWNTs hybrid nanocomposite samples with fixed nanofiller weight fraction (0.5 wt. %) and different mixing ratio.



Figure 8. Water absorption vs.GNPs-MWNTs nano-fillers with fixed weight fraction (0.5 wt. %) at different mixing ratio

The water absorbency of Epoxy/ GNP-MWNNT nanocomposite is smaller than that of Epoxy/ GNP nanocomposite and higher than that of Epoxy/MWNTs, because GNPs have natural tendency to absorb water more than MWNTs and also due to higher exposed surface area of nanoplatelets [23]. Epoxy/ MWNTs nanocomposite is more hydrophobic than Epoxy/GNP-MWNT and Epoxy/GNPs nanocomposite. This is supported by contact angle measurement. And also GNPs created tortuous pathway in epoxy to defuse the water molecule inside the nanocomposite because it has high aspect ratio [24].

4. Conclusions

Direct mixing, which include mechanical mixing and high shear mixing followed by sonication, is experimental method used to prepare epoxy/GNPs-MWCNTs hybrid nanocomposites. This method showed Good improvement in stability and dispersion of GNPs-MWCNTs in epoxy with low cost, environmental friendly and fast. The Young's modulus of the epoxy/GNPs was 62% greater than the neat epoxy as compared to 6% increase for MWNTs. The increase in the ultimate tensile strength is 59% for Epoxy/GNPs, 27% for Epoxy/MWCNTs, as compared with that of the neat epoxy. The best improvements in mechanical properties of was found at two mixing ratios of GNPs: MWNTs (5:5) and (9:1), where ultimate tensile strength of the Epoxy/GNPs-MWNTs with mixing ratio (5:5) and (9:1) was 53% and 60% greater than the neat epoxy respectively. The fracture surface of tensile sample of epoxy/0.5 wt% GNPs nanocomposite indicates that GNPs have uniform good dispersion without agglomeration. For epoxy/ GNPs-MWNTs hybrid naocomposites, the fracture surface

indicates that the GNPs with MWNTs form 3-D hybrid architectures structure which inhibits face-face aggregation of GNPs. The hydrophobicity of Epoxy/0.5 wt% MWNTs is higher than that for epoxy/0.5 wt% GNPs where contact angles are (60.5° and 44.5°) and water absorption are (0.43% and 0.55%) respectively. Hydrophilicity of neat epoxy decreases by adding 0.5 wt.% GNPs-MWNTs with mixing ratio 2.5:7.5 where contact angles are changed from 43.5° to 79.5°. Thermogravimetric analysis results for neat epoxy, Epoxy/MWNTs, Epoxy/GNPs, and Epoxy/GNPs-MWNTs do not show any major influence on thermal stability of epoxy.

REFERENCES

- D. Galpaya, M. Wang, M. Liu, N. Motta, E. Waclawik and C. Yan, 2012, "Recent Advances in Fabrication and Characterization of Graphene-Polymer Nanocomposites," Graphene, Vol. 1, No. 2, pp. 30-49.
- [2] E. E. Tkalya, M. Ghislandi, G. De With, C. E. Koning, 2012, "The use of surfactants for dispersing carbon nanotubes and graphene to make conductive nanocomposites," Current Opinion in Colloid & Interface Science, Vol. 17, pp. 225-232.
- [3] G. De Bellis, A. Tamburrano, A. Dinescu, M. L. Santarelli, M. S. Sarto, 2011, "Electromagnetic properties of composites containing graphite nanoplatelets at radio frequency," Carbon, vol. 49, pp.4291-4300.
- [4] S. Iijima, 1991, "Helical microtubules of graphitic carbon," Nature, Vol. 354, pp. 56–58.
- [5] K. S. Novoselov, A. K. Geim, S. V. Morozov, D. Jiang, Y. Zhang S. V. Dubonos, V. Grigorieva and A. A. Firsov, 2004, "Electric Field Effect in Atomically Thin Carbon Films," Science, Vol. 306, pp.666-669.
- [6] P. M. Ajayan, 1999 "Nanotubes from Carbon, Chemical Reviews," Vol. 99, pp. 1787-1799.
- [7] R. S. Ruoff, D. Qian and W. K. Liu, 2003 "Mechanical properties of carbon nanotubes: theoretical predictions and experimental measurements," C. R. Physique, Vol. 4, pp. 993-1008.
- [8] J. Pu, S. Wan, Z. Lu, G. Zhang, L. Wang, X. Zhangb and Q. Xue, 2013, "Controlled water adhesion and electrowetting of conducting hydrophobic graphene/carbon nanotubes composite films on engineering materials," Materials Chemistry, Vol.1, pp.1254–1260.
- [9] T. W. Ebbesen, H. J. Lezec, H. Hiura, J. W. Bennett, H. F. Ghaemi and T. Thio, 1996, "Electrical conductivity of individual carbon nan- otubes," Nature, Vol. 382, pp. 54-56.
- [10] S. Stankovich, D. A. Dikin, G. H. B. Dommett, K. M. Kohlhaas, E. J. Zimney, E. A. Stach, R. D. Piner, S. T. Nguyen and R. S. Ruoff, 2006, "Graphene-based composite materials," Nature, Vol.442, pp.282-286.
- [11] S. Y. Yang, W. N. Lin, Y. L. Huang, H. W. Tien, J. Y. Wang, C. C. Ma, S. M. Li, 2011, "Synergetic effects of graphene platelets and carbon nanotubes on themechanical and

thermal properties of epoxy composites," Carbon, Vol.49, No.3, pp.793-803.

- [12] R. Verdejo, M. M. Bernal, L. J. Romasanta and M. A. Lopez Manchado, 2011, "Graphene Filled Polymer Nanocomposites," Materials Chemistry, Vol. 21, No. 10, pp. 3301-3310.
- [13] A. A. Moosa, F. Kubba, Maysam Raad and A. Ramazani S. A, 2016, Mechanical and Thermal Properties of Graphene Nanoplates and Functionalized Carbon-Nanotubes Hybrid Epoxy Nanocomposites, American Journal of Materials Science, Vol.6, No.5 pp. 125-134, DOI: 10.5923/j.materials.20160605.02.
- [14] P. Wang, T. Hsieh, C. Chiang, and M. Shen, 2015, "Synergetic Effects of Mechanical Properties on Graphene Nanoplatelet and Multiwalled Carbon Nanotube Hybrids Reinforced Epoxy/Carbon Fiber Composites, J. of Nanomaterials, Vol.2015, pp.1-10.
- [15] M. R. Ayatollahi, M. M. Shokrieh, S. Shadlou, A.R. Kefayati, and M. Chitsazzadeh, 2011, "Mechanical and electrical properties of epoxy/multi-walled carbon nanotube/ nanoclay nanocomposites," Iran Polymer, Vol. 20, pp. 835-843.
- [16] B. A. Moghadam, 2015, "Development of A Highly Resilient Graphene Nanoplates Resin/Adhesive," Ch 2, pp.19.
- [17] S. Singh, V. K. Srivastava, and R. Prakash, 2013, "Characterization of multiwalled carbon nanotube reinforced epoxy resin composites," Mater Sci Technol Vol.29, No.9, PP.1130–1134.

- [18] A. A. Balandin , S. Ghosh, W. Bao, I. Calizo, D. Teweldebrhan, F. Miao and C. N. Lau, 2008, "Superior thermal conductivity of single-layer graphene," Nano Lett, Vol. 8, pp.902-907.
- [19] P. Kim, L. Shi, A. Majumdar, and P.L. McEuen, 2001, "Thermal transport measurements of individual multiwalled nanotubes," Phys. Rev. Lett, Vol. 87, pp. 215502.
- [20] S. Paszkiewicz, 2014, "Polymer Hybrid Nanocomposites Containing Carbon Nanoparticles In Situe Synthesis and Physical Properties, West Pomeranian University of Technology, Szczecin, Poland," PhD Thesis.
- [21] I. A. Mir and D. Kumar, 2012 "Carbon nanotube-filled conductive adhesives for electronic applications," Nanoscience Methods Vol. 1, pp.183–193.
- [22] M. T. Le and S. Ch. Huang, 2015, "Thermal and Mechanical Behavior of Hybrid Polymer Nanocomposite Reinforced with Graphene Nanoplatelets Materials," Vol. 8, pp.5526-5536.
- [23] I. Zaman, Sh. Araby, B. A. Khalid, Manshoor, 2014, "Moisture Absorption and Diffusivity of Epoxy Filled Layered-Structure Nanocomposite," Vol. 8, pp. 2626–2631.
- [24] H. Zhao, R. K. Y. Li, 2008, "Effect of water absorption on the mechanical and dielectric properties of nano-alumina filled epoxy nanocomposites," Compostie Part A Applied Science Manufacture, Vol. 39, pp. 602–611.