

MLD Model of Boiler-Turbine System Based on PWA Linearization Approach

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Abstract In this paper we consider boiler-turbine's nonlinear dynamics and linearize the nonlinear parts based on the piecewise affine method in order to obtain a mixed logical dynamical model of the system. By using piecewise affine approach for linearization of the system's nonlinear equations, the obtained linearized model switches between different modes based on its parameters, so acquired piecewise affine model can be categorized in the switching hybrid system class. We model the linearized boiler-turbine system in a mixed logical dynamical model of the hybrid systems using hybrid system's description language and hybrid toolbox. Mixed logical dynamical model describes system by two linear equations and one linear inequality with a reasonable accuracy and considering the constraints in the system. We provide a comparison between the acquired mixed logical dynamical model using piecewise affine linearization method and the actual boiler-turbine system through simulation and show the efficiency of the mixed logical dynamical model to describe the Boiler-Turbine system.

Keywords Boiler-Turbine System, Hybrid System, Piecewise Affine Method, Mixed Logical Dynamical Model, Modelling Nonlinear System

1. Introduction

In the study of power systems having a desirable model of system is important. A boiler-turbine system is an energy conversion system that consists of a steam boiler and a turbine which uses chemical energy to generate electricity. Boiler-turbine system model first was represented at 1972 using nonlinear equations based on the boiler-turbine plant P16/G16 at the Sydsvenska Kraft AB Plant in Malmo, Sweden[1]. A schematic diagram of the boiler-turbine unit is shown in Figure.1. After that the boiler-turbine's nonlinear model was studied widely in many articles and was undergone a number of amends to provide a better description of system[2,3]. In order to design a controller some researchers used nonlinear form of system's equations[5,6, 10] and in other works the linear form of the system was used[4,7-9].

The boiler-turbine system can be modeled as a multi-input multi-output (MIMO) nonlinear system. This system is strongly coupled and is subject to various constraints on both inputs and outputs. In literatures that used the linearized form of boiler-turbine system, they obtained a linearized model using a truncated Tylor series expansion of nonlinear

equations around operating points[4,7-9]. Linearization around operating points provides a relatively accurate description about system behaviour around these points, however for using of this method we should have nominal states' and inputs' values at operating points which are not readily available.

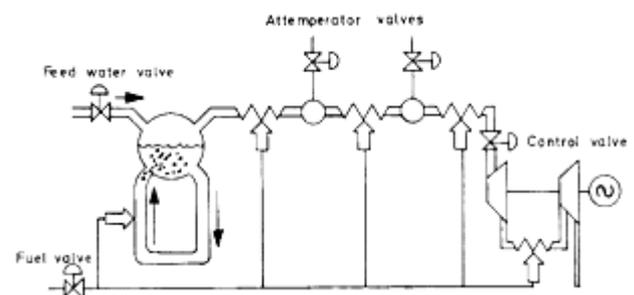


Figure 1. schematic diagram of the boiler-turbine unit

Because of improvement in computational methods and hardware, today the control's technology is moving toward intelligent and computer based controller methods namely model predictive control. For using such control methods, we need to provide a model of system which describes the system's behaviour properly. A good way for providing a proper model of different classes of systems is using hybrid system's modelling approach specially mixed logical dynamical (MLD) method which describes system using two linear equations and one linear inequality. In order to obtain a MLD model of a system first the system's equations need

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to be linearized, so we use piecewise affine (PWA) approach for linearization in which the space is divided into different pieces and in each section a linear equation is used for description of system behaviour in that section[11].

Here we use the boiler-turbine's nonlinear equations which represented in[3], to obtain a linear model of boiler-turbine system in the mixed logical dynamical framework using piece wise affine approach for linearization. The rest of the paper is as follows. In Section 2, we introduce the mathematical model of the boiler-turbine system and use piecewise affine method for linearization. Next in section 3, we acquire a MLD model and provide simulations and comparisons of the achieved MLD model and the actual system in identical condition. Finally, concluding remarks are drawn in Section 4.

2. Mathematical and Linear Model of Boiler-Turbine System

In this section, we consider the boiler-turbine system's continuous-time dynamical equations as follow[3]:

$$\frac{dp}{dt} = -0.0018u_2p^{9/8} + 0.9u_1 - 0.15u_3 \quad (1-1)$$

$$\frac{dp_0}{dt} = (0.073u_2 - 0.016)p^{9/8} + 0.1p_0 \quad (1-2)$$

$$\frac{dp_f}{dt} = \frac{(141u_3 - (1.1u_2 - 0.19)p)}{85} \quad (1-3)$$

where p , p_0 and p_f are drum pressure (kg/cm^2), power output (MW) and fluid density (kg/cm^3), respectively. The inputs to the system are u_1 , u_2 and u_3 which respectively indicate to fuel flow valve position, steam control valve position and feedwater flow valve position, and have a value in the interval $[0,1]$. Changes in valves' position have the following limitations:

$$\left| \frac{du_1}{dt} \right| \leq 0.007/sec \quad (2-1)$$

$$-2/sec \leq \frac{du_2}{dt} \leq 0.007/sec \quad (2-2)$$

$$\left| \frac{du_3}{dt} \right| \leq 0.05/sec \quad (2-3)$$

The output to the system are p , p_0 , and X_w which are respectively drum pressure, output power, and drum water level (in meters). Two first output are system's states and readily available, whereas water level is found through the following relationships:

$$X_w = 0.05(0.13073p_f + 100\alpha_{cs} + \frac{q_e}{9} - 67.975) \quad (3-1)$$

$$\alpha_{cs} = \frac{(1 - 0.001538p_f)(0.8p - 25.6)}{p_f(1.0394 - 0.0012304p)} \quad (3-2)$$

$$q_e = (0.854u_2 - 0.147)p + 45.59u_1 - 2.514u_3 - 2.096 \quad (3-3)$$

where q_e is the evaporation rate (kg/sec) and α_{cs} is the steam quality.

For obtaining the MLD model of the boiler-turbine system according equations (1), (3) and by using Hybrid Systems Description Language (HYSDEL), first the nonlinear terms in these equations must be omitted. These nonlinear terms are presented at equation (4).

$$f_1(p, u_2) = u_2p^{9/8}, \quad f_2(p, u_2) = u_2p, \\ f_3(p, p_f) = \frac{(1 - 0.001538p_f)(0.8p - 25.6)}{p_f(1.0394 - 0.0012304p)} \quad \text{and} \quad f_4(p) = p^{9/8} \quad (4)$$

As we mentioned earlier, for linearization we use the PWA approach[11]. So we considered that the p , p_f and u_2 respectively have a value in the interval $[70,145]$, $[200,600]$, and $[0,1]$ which describe operating space of boiler-turbine system, and divide each space into the 4 equal separate sections. In consequence, the nonlinear terms f_1 , f_2 , and f_3 consist 16 sections and f_4 consists 4 sections. Now we describe the nonlinear terms in each section with a linear equation. For f_1 , f_2 , and f_3 we represent nonlinear terms using surfaces as follow:

$$z = a_i x + b_i y + c_i \quad i=1, \dots, 16 \quad (5-1)$$

and in order to describe f_4 we use linear lines with following equations:

$$y = \hat{a}_i x + \hat{b}_i \quad i=1, \dots, 4 \quad (5-2)$$

where a_i , b_i , \hat{a}_i and \hat{b}_i are constant factors related to the i -th section.

For example according to equation (5-1) the surface which describes the nonlinear terms f_3 in the interval $p_f=[300,400]$ and $p=[107.5,126.3]$ is as follow:

$$f_3 = (-0.0006.327984)p_f + (0.0013753)p + (0.16542755)$$

similarly, we can obtain the linear form of equations (4) in each section. Comparisons between nonlinear and linear form of f_1 , f_2 , f_3 , and f_4 are shown in Figure.2.

Now according to linearized form of nonlinear terms, the boiler-turbine system's dynamics can be written in the PWA configuration which Equation (6) shows general formulation of that[11].

$$x_{k+1} = A_i x_k + B_i u_k + h_i \quad \text{if } \Omega_i = \text{true} \quad (6) \\ y_k = C_i x_k + D_i u_k + g_i$$

where, k is the discrete-time step. x , u , and y denote states, inputs, and outputs, respectively. Ω_i indicates a set of conditions which defines i -th section of space (for boiler-turbine we have 64 section). A_i , B_i , h_i , C_i , D_i , and g_i are proper time-invariant matrix related to section i . The concept of PWA model is depicted in Figure.3.

In next section according to the linear discrete-time equations of boiler-turbine system, which were obtained in this section, and using HYSDEL we will acquire the MLD model of system.

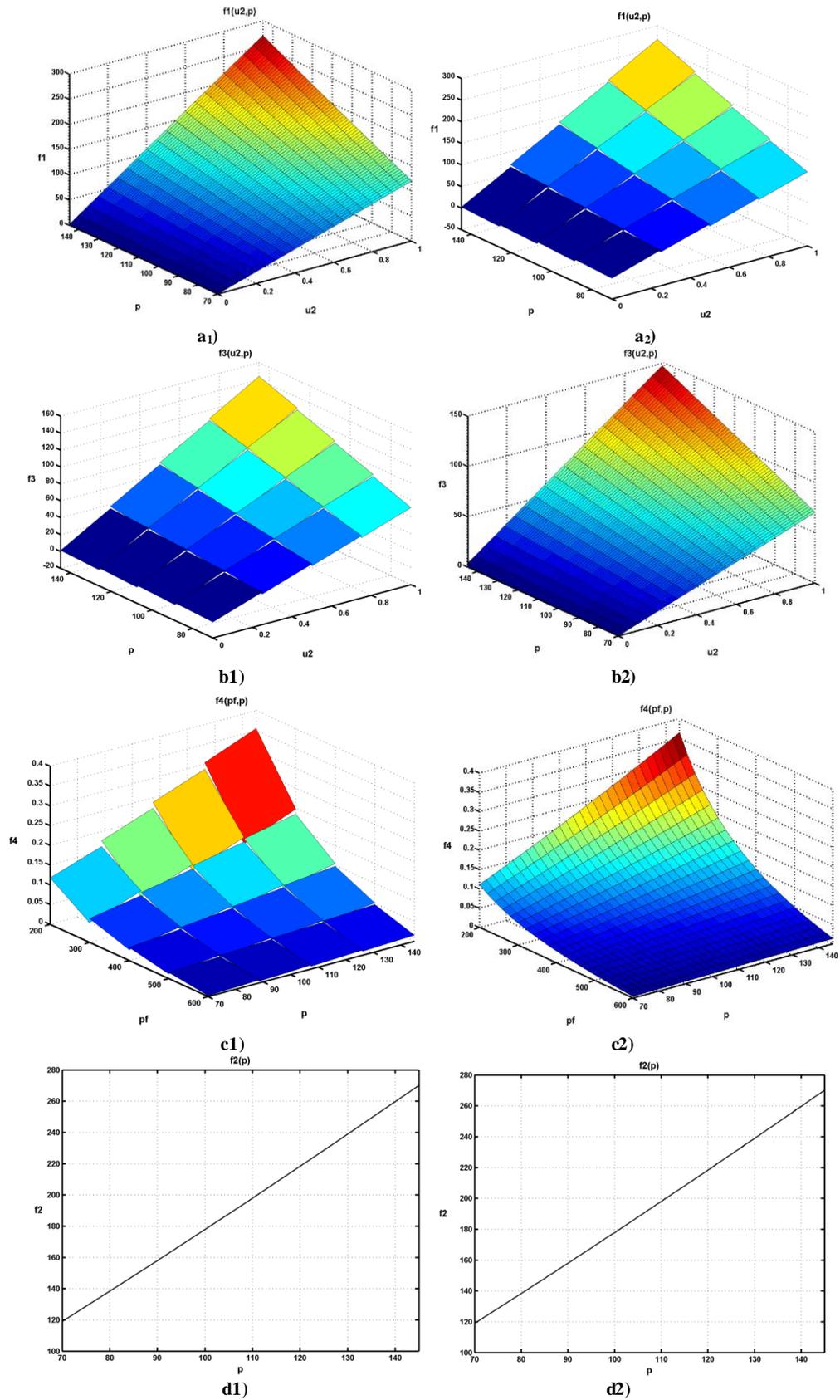


Figure 2. comparison between nonlinear and linear form of f_1 (a), f_2 (b), f_3 (c), and f_4 (d): left pictures are showed linearized form and right pictures are showed nonlinear form

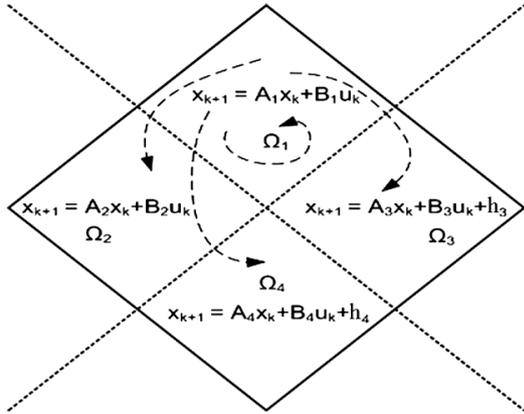


Figure 3. a bounded PWA model: in each section linear dynamics describe system behaviour

3. Mixed Logical Dynamical Model and Simulation

There are many different methods for modelling of hybrid system, namely Piecewise affine, Mixed logical dynamical, Linear complementarity, and Max-min-plus-scaling[12].

Among these models, MLD method is more common and has less complexity than other methods which models hybrid system using two linear equations (7-1) and (7-2) and one linear inequality (7-3). MLD approach has the following structure[13]:

$$x(k+1) = Ax(k) + B_1 u(k) + B_2 \delta(k) + B_3 z(k) \quad (7-1)$$

$$y(k) = Cx(k) + D_1 u(k) + D_2 \delta(k) + D_3 z(k) \quad (7-2)$$

$$E_2 \delta(k) + E_3 z(k) \leq E_1 u(k) + E_4 x(k) + E_5 \quad (7-3)$$

where $x = [x_c \ x_l]^T$, $x_c \in R^{n_c}$, $x_l \in \{0,1\}^{n_l}$ is the system state, $y = [y_c \ y_l]^T$, $y_c \in R^{p_c}$, $y_l \in \{0,1\}^{p_l}$ and

$u = [u_c \ u_l]^T$, $u_c \in R^{m_c}$, $u_l \in \{0,1\}^{m_l}$ are the output and the input signal, respectively. $\delta \in \{0,1\}^{r_l}$ denotes the logical auxiliary variables, and $z \in R^{r_c}$ denotes the continuous auxiliary variables. The indexes c and l represent the type of the variables and respectively indicate continuous and logical. A , B_i , C , D_i and E_i are proper and time-invariant matrixes.

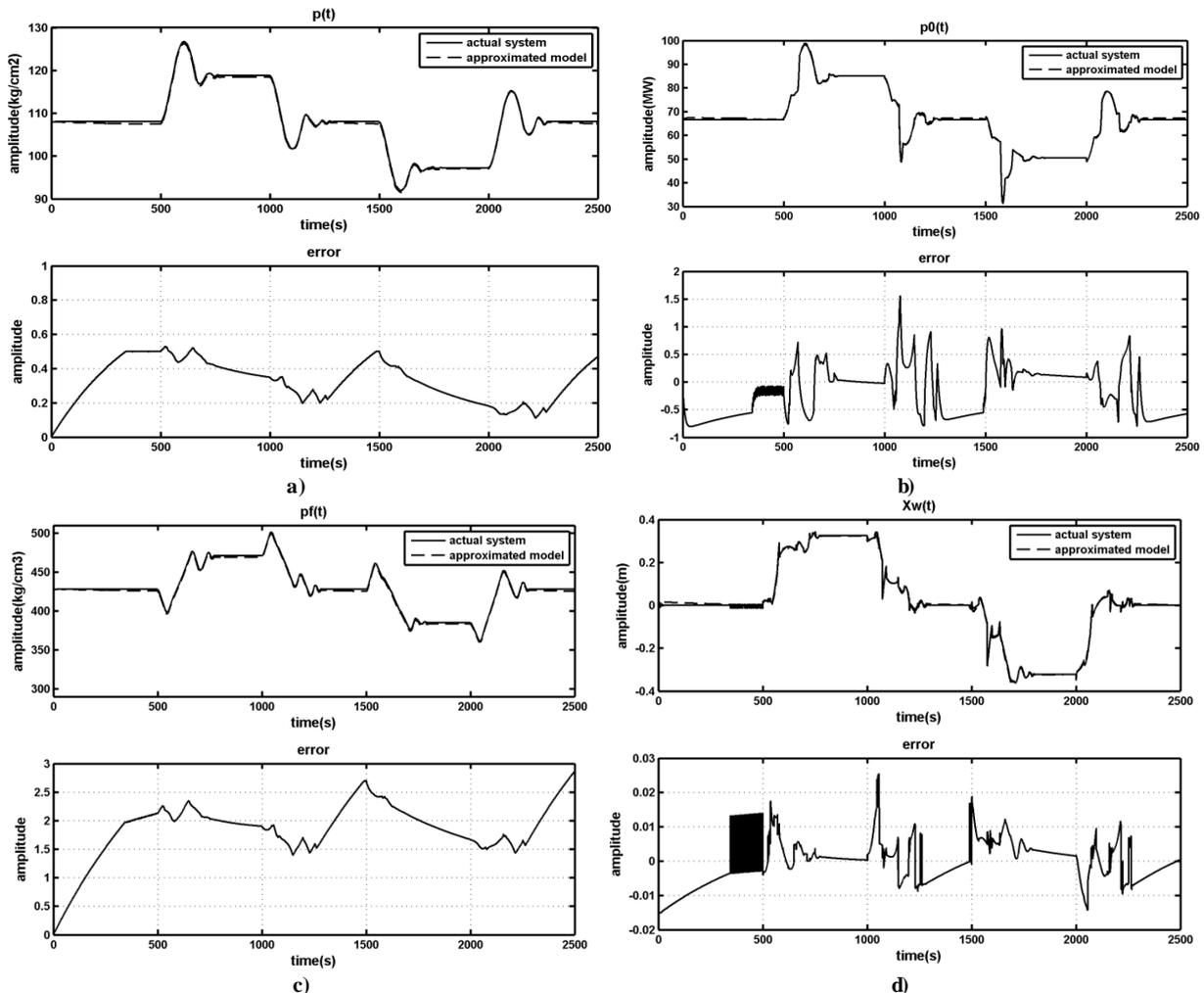


Figure 4. actual system's states and outputs (solid-line) in comparison of MLD model's states and outputs (dashed-line) under identical conditions and inputs' signals: a)drum pressure, b) power output, c)fluid density, and d)drum water level

Before obtaining the MLD model of boiler-turbine system based on the PWA model (equation (6)), in order to impose the inputs' constraints that were defined at equations (2); we introduce 3 new states (8-1) and 3 new equations (8-2) as follow:

$$pu_i(k + T_s) = u_i(k) \quad i = 1, 2, 3 \quad (8-1)$$

$$du_i(k) = \frac{u_i(k) - pu_i(k)}{T_s} \quad i = 1, 2, 3 \quad (8-2)$$

where T_s is sampling time. pu and du denote the new state variable and input's pace, respectively.

Now the MLD model (7) of boiler-turbine system is obtained by using HYSDEL and hybrid toolbox [14, 15]. The MLD model of the system by using PWA method for linearization has the following properties:

1. Sampling time (T_s) is 1s.
2. 6 states (6 continuous: -0 binary), 3 inputs (3 continuous: -0 binary), 3 outputs (3 continuous: -0 binary).
3. 63 continuous auxiliary variables, 45 binary auxiliary variables, 392 mixed-integer linear inequalities.

In following, we provide a comparison between approximated MLD model and actual system under identical conditions and inputs signals. The results of simulation are shown in Figure.4.

By looking at Fig.4, it is obvious that using piecewise affine approach for linearization describes actual system behavior at a reasonable accuracy level. In order to increase the accuracy of the MLD model of boiler-turbine system we should increase the number of partitions of the piecewise affine approach. However according to the MLD models' properties, we should consider that increase in partitions' number causes increase in the number of auxiliary variables and mixed-integer linear inequalities related to the MLD model. Consequently, we need more computational effort to use this MLD model in order to design a controller for the actual boiler-turbine system

4. Conclusions

As we showed in this paper hybrid systems modelling approaches can be used not only for systems with inherently hybrid behaviours but also nonlinear systems, by using local linearization method namely PWA. We showed using MLD model method for modelling boiler-turbine system as a hybrid system makes us able to impose constraint directly into the system model and provides a very simple, systematic, and relatively accurate model of system. This accuracy comes from the PWA method which we used for linearization of nonlinear terms but increase in accuracy also causes increase in computational effort for designing a proper controller based on the MLD model. So we should make a balance between accuracy and computational cost according to our purposes and available equipments.

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