

Comparative Study of the Copper Electrical Earthing Corrosion in Three Mediums in Senegal

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Abstract A electrical earthing is a low-resistance metallic electrode in close contact with the earth, which is able to conduct default and leaking electric current to the earth. A good electrical earthing allows current circulation through the earth and protects equipments and persons from electrical risks. In Senegal a foundation earthing with a loop system onto the bottom of building excavation is used on a high majority of new buildings in construction. The same copper is used in all sites for all kinds of buildings (office, school, commercial or medical use). The corrosion resistance of the copper grounding in the soil is very important for the safety and power operation. A quick consumption of copper by corrosion with the presence of electrolyte (natural water exposure) can occur a matter of safety. We purpose to study the corrosion rates in different water exposures. This work is about a comparative corrosion rates of a copper electrical earthing in different mediums. Those mediums of study are the exposure of three aqueous environments: city water, rainwater and seawater. The purpose of the work is to assess and compare this earthing corrosion rates in those various environments and found the more aggressiveness solution or medium. The physico-chemical datas of aqueous solutions were analyzed and summarized before electrochemicals measurements. The open circuit potential (OCP) is accessed by chronopotentiometry after 2 hours of potential monitoring. The linear polarization with Evans diagram and Tafel extrapolation methods were performed. Those methods show the kinetics of corrosion of copper earthing in city water, seawater and rainwater. The results showed a higher corrosion rate in seawater (32 $\mu\text{m}/\text{year}$) and low corrosion rates in city water and rainwater (ranging about 2 and 3 $\mu\text{m}/\text{year}$). For more security of persons and equipments copper earthing require in sea areas more thickness or more control or replacements. This study contributes to increase the safety of electrical power in buildings.

Keywords Copper electrical earthing, Rainwater, Seawater, City water, Corrosion rate

1. Introduction

A electrical earthing is a low-resistance metallic electrode in close contact with the earth, which is able to conduct default and leaking electric current to the earth with low frequency (low voltage network in 50 Hz alternating current) or high frequency (lightning current) as defined by Lim *et al* [1]. Those electrical earthing are used with a foundation earth electrode or a simple vertical earth rod in general. In the context of our study (Senegal), most of the earthing are in copper looping. Many works devoted to the study of those groundings and related to the soils' resistivity reduction, thus permitting to improve the earthing quality (lower electric resistance) are available in the literature [2-11]. In contrast, only few works are focused between the correlation of the

earthing corrosion and the increase of the earth's [12] conductivity. In Senegal copper looping is generally used in all sites for new buildings for office, schools, hospitals, administration, banks, etc. Due to the importance of the corrosion resistance for durability and safety for persons and equipments it is necessary to show the corrosion rates of copper earthing for different mediums. A higher corrosion rate can contribute to a rapid consumption or a disappearance of the electrical earthing protection with negation consequence for human and equipment safety. This paper sets out the corrosion rates in rainwater, city water and seawater of a 29 mm² copper earthing. Due to the presence of water in soil our study shows the influence of water quality (city water, rainwater and seawater) on the copper electrical earthing corrosion.

The study can clarify if it is judicious to use copper as a electrical earthing in all sites exposures. The criteria of corrosion rates comparison is used for solving our problematical. Three methods were used for investigations.

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First the physico-chemicals analysis allow to show different parameters of aqueous solutions as temperature, pH, conductivity, total hardness, anions and cations concentrations. The second method is the chronopotentiometry in zero current for determination of the free-corrosion potential or open circuit potential (OCP) of copper in the mediums of study for 2h. The third method set out the Evans and Tafel extrapolations diagrams with the corrosion by polarization for ± 500 mV Ag/AgCl around the OPC. Experimental results will permit to compare the copper corrosion rates in the different environments and set out the most aggressiveness medium.

The study can be beneficial for electrical technicians and humans to increase the safety in many buildings in Senegal.

2. Experimental

2.1. Material

The electrochemical measurements were performed on 29 mm² samples cut from pure (99%) bare copper of earthing. These copper samples were used as working electrodes, Ag/AgCl in saturated KCl was used as the reference electrode, and the counter-electrode was a large stainless steel grid.

2.2. Solutions

Basically, buried metal corrosion, has an electrochemical nature due to the presence of electrolyte in the earth [13]. The solutions under study are city water, seawater and rainwater. The physicochemical characteristics of these solutions are summarized in Table 1. The pH, temperature and conductivity were determined by measurements with standard equipment. The other parameters were carried out by calorimetry.

We should mention that rainwater used in this study was directly collected, before any contact with the land. This rainwater is different from the other run-off or infiltration waters definitions [14]. Those waters can be loaded with various contaminants like hydrocarbons from paved roads deteriorations, minerals, organic components or microorganisms, etc. [15, 16].

Table 1. Physicochemical characteristics of the solutions under study

	City water	Rainwater	Seawater
pH	7.1	6.5	8.5
Temperature (°C)	26	26	26
Conductivity ($\mu\text{S cm}^{-1}$)	441	686	53436
Total hardness (10^{-4} mol L ⁻¹)	16	5	412.5
Cl ⁻ (mg L ⁻¹)	8	2.26	27512.5
NO ₃ ⁻ (mg L ⁻¹)	3.4	0.07	0
SO ₄ ²⁻ (mg L ⁻¹)	21	2.42	312
Na ⁺ (mg L ⁻¹)	35	3.36	7086.75
K ⁺ (mg L ⁻¹)	12.2	0.57	338.1

2.3. Experimental Methods

The copper sample corrosion was investigated by *chronopotentiometry and linear dynamic polarization methods* [17] using a Potentiostat/Galvanostat μ -Autolab III controlled by the GPES (General Purpose for Electrochemical System) software. The external surfaces of the metal samples were first sandpapered with abrasive papers (P 300 and P 800 successively) to remove the surface oxides layers before rinsing them using a squeeze bottle of distilled water.

The open-circuit potential was determined by *chronopotentiometry* for 2 hours, after a period of stabilization of 30 minutes. *Linear polarization (Evans diagram and Tafel extrapolations)* consists of polarizing the electrode in the domain $E_{\text{corr}} \pm 500$ mV, then in fitting the experimental values into the Tafel lines. This method permits to obtain the corrosion kinetics data (corrosion rate, potential and current of corrosion, Tafel slopes, etc.) [18]. The measurement is done subsequently to the free-corrosion potential measurement. The scanning rate was 1 mV s⁻¹ in the explored potential field for 1 cycle by linear polarization for ± 500 mV Ag/AgCl around the OCP. The samples surfaces were measured and specified in the operating software data.

3. Results and Discussion

Free-corrosion potential monitoring in various environments, as shown in **Fig. 1**, is more anodic in rainwater with a value close to -0.05 V/Ag/AgCl. In this case, the potential slightly increases from -0.06 to -0.04 V/Ag/AgCl between 0 and 1470 seconds. This step may correspond to a passivation of the metal due to the formation of a passive film on the electrode. From 1470 to 7200 s, the potential is almost constant (≈ -0.045 V/Ag/AgCl). The low presence of aggressive halogen anions and the low conductivity in rainwater (**Table 1**) are compatible with a low tendency for corrosion which explains the more anodic potential in this solution.

Fig. 1 shows that the most cathodic free-corrosion potential is obtained in seawater (about -0.22 V/Ag/AgCl). The potential rapidly decreases (from -0.12 to -0.22 V/Ag/AgCl) from 0 to 540 seconds in the first minutes, may be due to the dissolution of an oxide film that was formed on the surface [19]. From the 540 seconds to 7200 s, the potential stabilizes at around -0.22 V Ag/AgCl. The copper turns passive in this solution in which a blue coloration appears indicating a formation of Cu²⁺ ions. The important chloride concentration in seawater and its high conductivity (**Table 1**) explain the seawater aggressiveness (corrosion) [1] and the more cathodic potential.

Fig. 1 shows that the free-corrosion potential in city water (about -0.18 V/Ag/AgCl) is between those in seawater and rainwater. From 0 to 368 seconds, the potential decreases from -0.12 to -0.19 V/Ag/AgCl, and remains quite constant after (-0.18 V/Ag/AgCl). As for the ions concentrations, the

potential value is comprised between those obtained in seawater and rainwater, Anions in city water are related to human consumption water's treatment products. The corrosion kinetics was also investigated by plotting Evans Diagrams and Tafel extrapolations in the various environments.

Fig. 2 confirms that the most cathodic corrosion potential is obtained in seawater (about -0.29 V/Ag/AgCl) and the most anodic one in rainwater (about -0.08 V Ag/AgCl). The corrosion potential in city water is between the values obtained in rainwater and seawater (about -0.23 V Ag/AgCl). This is in accordance with the free-corrosion potential measurement results. The anodic branch shows a more important corrosion current density in seawater with an increase of $2.78 \mu\text{A}/\text{cm}^2$ to $0.018 \text{ A}/\text{cm}^2$ between -0.29 and 0.09 V Ag/AgCl potentials. The anodic branch is round shape in rainwater corresponding to an increase of current

density from $0.04 \mu\text{A}/\text{cm}^2$ to $29.6 \mu\text{A}/\text{cm}^2$ between 0.07 to 0.38 V Ag/AgCl potentials. In city water, the anodic branch follows the same behaviour as into rainwater with a part which current density increase is more rapid ($0.05 \mu\text{A}/\text{cm}^2$ to $110 \mu\text{A}/\text{cm}^2$) between -0.22 to 0.12 V Ag/AgCl potentials. The slopes of anodic curves (**Fig. 2**) are more important in city water and in rainwater. Then the current of corrosion is more emphasized, respectively in seawater. The additions of material like salt or components rich in chloride improve the soil conductivity (as in seawater) and contribute to increase copper earthing corrosion [1]. This analysis is in line with the conclusions obtained on the free corrosion potentials study. The Tafel datas analysis in **Table 2** show that the corrosion rate in seawater ($31.85 \mu\text{m}/\text{year}$) is about 14 times more important than the one obtained in city water ($2.23 \mu\text{m}/\text{year}$) and 11 times higher than rainwater ($2.77 \mu\text{m}/\text{year}$).

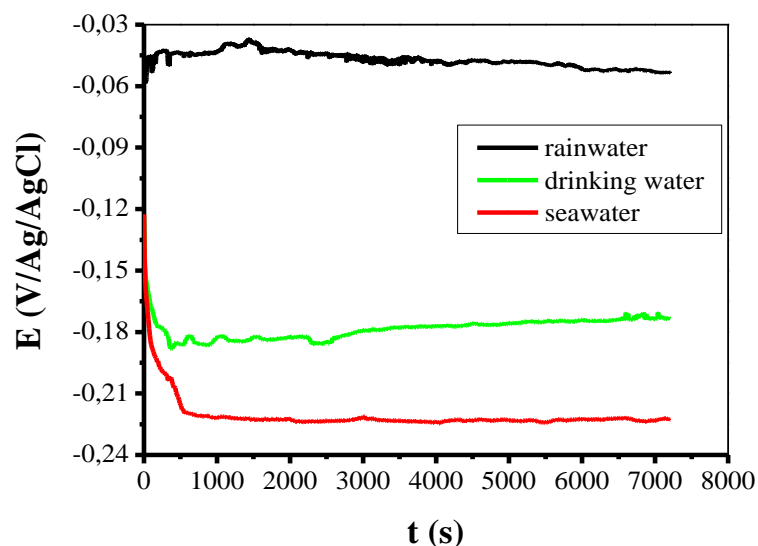


Figure 1. Copper free-corrosion potential evolution for 2 hours in the three studied environments

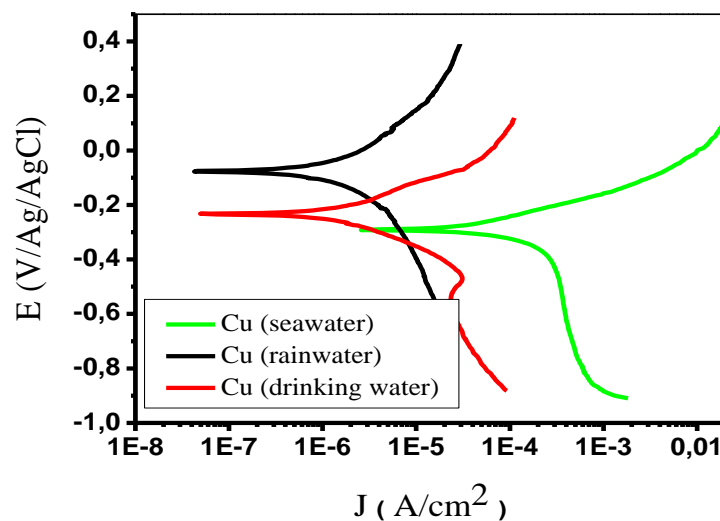


Figure 2. Evans diagram of copper in various mediums

Table 2. Tafel datas for copper in various environments

Datas	Rainwater	City water	Sea water
Observed E_{corr} (V/Ag/AgCl)	-0.077	-0.233	-0.292
calculated E_{corr} (V/Ag/AgCl)	-0.085	-0.235	-0.283
J_{corr} ($\mu\text{A}/\text{cm}^2$)	3	1	31
I_{corr} (μA)	3	2	31
R_p to E_{corr} (Ω)	$300.3 \times 10^{+2}$	$92.2 \times 10^{+2}$	$3.9 \times 10^{+2}$
R_p (Ω)	$383 \times 10^{+2}$	$32 \times 10^{+2}$	100
Corrosion rate (mm/year)	2.77	2.23	31.85
β_a (V/dec.)	0.43	0.12	0.09
β_c (V/dec.)	-0.61	-0.12	-0.09
Samples surface (cm^2)	1	1.8	1

Corrosion current densities are respectively more important into seawater ($31.15 \mu\text{A}/\text{cm}^2$), then into rainwater ($3 \mu\text{A}/\text{cm}^2$), and finally into city water ($1.1 \mu\text{A}/\text{cm}^2$).

The higher corrosion rate in seawater confirms the idea of catalyzing process of corrosion by salt and water in areas near the beach [1].

Copper corrosion in an electrical earthing or its breaking puts people and equipments at electric risks [1]. Then the use of copper as a general material for electrical earthing in all sites is not judicious. The possible presence of a default current or alternative nature leakage flowing through the grounded towards the earth would not significantly affect the corrosion [20], which testifies for those currents not being considered in our study.

4. Conclusions

The study show a electrical risk for persons and equipments with higher corrosion of copper earthing in sea areas as in Senegal context. Copper potential is more cathodic into seawater (presence of chlorides), and more anodic in rainwater. The corrosion rate is especially higher in seawater ($32 \mu\text{m}/\text{year}$). It is at least ten times more intense relatively to city water or rainwater. Copper earthing corrosion into city water and rainwater is quite the same according to the Tafel results (ranging about 2 and 3 $\mu\text{m}/\text{year}$).

Then the use of copper as a general material of electrical earthing in all sites as in Senegal is not judicious. The extended use of copper as a electrical earthing raises the issue of durability and must go together with specific measures into seawater (more important thickness or more frequent checking).

Thus, soil conductivity improvement solutions through addition of material like salt or components rich in chloride will contribute to increase copper earthing corrosion. This solution is not good for copper corrosion in spite of the reducing of the resistance of copper earthing. As in sea areas this method increasing the conductivity of soil is not judicious due to the risk of important corrosion.

Ours study shows a risk of higher corrosion in sea area and in earthing with chlorides addition. The risk is a disparation

of earthing by corrosion and compromise the function of electrical earthing with copper corrosion. The results contribute to increase more safety of copper earthing in electrical power for humans and equipments in the buildings.

The study's opened up prospects can include:

- The impact of bacteria [12] and other soils components influence (acidity, porosity, etc.) on the results. Bacteria that could worsen corrosion through their metabolism and acid secretions [1] or inhibit corrosion by the biofilm formed [21]; soils that can be rich in limestone or phosphate able to suppress corrosion (inhibition) [1].
- Increasing the number of samples (from 5 to 10) of study for more analytical datas. Corrosion in well water and waste water can be investigated.
- A comparative study of corrosion in the same mediums with stainless steel. Thus can inform to the relevance of the use of 304 stainless steel in earthing lightning protection as recommended by French standard recommendation [22], in aggressive soils.

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REFERENCES

- [1] S.C. Lim, C. Gomes, M.Z.A. Ab Kadir, International Journal of Electrical Power & Energy Systems, 47, pp. 117–128, 2013.
- [2] R.W. Nielsen, Reducing resistivity in an electrical grounding system. Utah, USA: Permanent Buildings and Foundations, 1995.
- [3] C. Gomes, C. Lalitha, C. Priyadarshane, Improvement of earthing systems with backfill materials. In: 30th International conference on lightning protection, vol. 1086. Italy: Cagliari, p.1–9, 2010.
- [4] M.B. Kostic, Z.R. Radakovic, N.S. Radovanovic, M.R. Tomasevic-Canovic, Improvement of electrical properties of grounding loops by using bentonite and waste drilling mud. IEE Proc – Generation, Transm Distrib Jan;146(1), p. 1–6, 1999.
- [5] W.R. Jones, Bentonite rods assure ground rod installation in problem soils. IEEE Trans Power Apparatus Syst ;PAS-99(4), p.1343–6, 1980.
- [6] H.E. Martínez, E.L. Fuentealba, L.A. Cisternas, H.R. Galleguillos and J.F. Kasaneva, de la Fuente OA. A new artificial treatment for the reduction of resistance in ground electrode. IEEE Trans Power Deliv; 19(2), p. 601–8, 2004.

- [7] E. George, C.J. Ekow and F.M. Tetteh, Palm kernel oil cake as an alternative to earth resistance – reducing agent. *Int J Appl Eng Res* ;4(1), 2009.
- [8] H. Yamane , T. Ideguchi, M. Tokuda and H. Koga, Long-term stability of reducing ground resistance with water-absorbent polymers. In: 1990 IEEE international symposium on electromagnetic compatibility, symposium record;p. 678–82, 1990.
- [9] J. He, G. Yu, J. Yuan, R. Zeng, B. Zhang and J. Zou, Decreasing grounding resistance of substation by deep-ground-well method. *IEEE Trans Power Deliv*; 20(2), p. 738–44, 2005.
- [10] Q.B. Meng, J. He, F.P. Dawalibi and J. Ma, A new method to decrease ground resistances of substation grounding systems in high resistivity regions. *IEEE Trans Power Deliv*; 14(3), p. 911–6, 1999.
- [11] A. Samouđian, I. Cousin, A. Tabbagh, A. Bruand, G. Richard, Electrical resistivity survey in soil science. A review. *Soil Till Res*; 83(2), p. 173–93, 2005.
- [12] L. O. A. Oyinkanola *and al.* (2016). Correlation between soil electrical resistivity and metal corrosion based on soil types for structural designs. pp 26-29.
- [13] S. Audisio and G. Beranger, Chapitre 7 in *Anticorrosion et durabilité dans le bâtiment, le génie civil et les ouvrages industriels*, Presses Polytechniques et Universitaires Romandes, 2010.
- [14] F. Valiron, *Gestion des eaux, principes-moyens-structures*. Presse de l'Ecole nationale des Ponts et Chaussées, Paris, 1990.
- [15] F. Valiron, Tabuchi J. P., *Maitrise de la pollution urbaine par temps de pluie : Etat de l'art*, Paris Tec et doc Lavoisier, p. 564, 1992.
- [16] M. Legret, V. Colandini, C. Le Marc, Effects of a porous pavement with reservoir structure on the quality of runoff water and soil. *Science of the Total Environment*, 189, pp. 335-340, 1996.
- [17] N. Perez, *Electrochemistry and corrosion science*, department of mechanical engineering university of Puerto Rico, kluwer academic publishers, New York, Boston, Dordrecht, London, Moscow, pp.71-118, 2004.
- [18] R.G Kelly, Chapter 2 in *Electrochemical Thermodynamics and Kinetics of Relevance to Corrosion*, electrochemical techniques in corrosion engineering, Marcel Decker inc., New York, pp. 9-54, 2003.
- [19] F.A. Martin, C. Bataillon, M.L. Schlegel, *Journal of Nuclear Materials* 379, p. 80, 2008.
- [20] J. Leconte, *Protection contre la corrosion. Techniques De L'ingénieur*, A830, p 1-22.
- [21] B. Mishra, Corrosion characterization of advanced steels for use in the oil and gas industry, *International Journal of Metallurgical Engineering, Scientific and Academic Publishing*, 2(2), pp 221-229, 2013.
- [22] NF C17-100: *Protection contre la foudre - Protection des structures contre la foudre - Installation de paratonnerres*, Indice de classement : C17-100,1997.