

About Possibilities of Strengthening of Epoxypolymer Composites by Modified Brick Powder

Dmitro L. Starokadomsky

O. O. Chuiko Institute of Surface Chemistry, Kyiv, Ukraine

Abstract The composites of the epoxypolymer (EP) with the brick powder (BP) are new materials that combine high characteristics with the low price. Herein we discuss about the several such compositions and evaluate some physical characteristics for them. Presented data suggest that BP (at the concentration range from 5 to 50 wt%) increases strength characteristics of the epoxypolymer's compression and abrasion, and reduce his shrinkiness. At the same time, the BP in 10 wt% concentration leads to the frustration and defectation in composite structure. Under the high concentrations of the BP (50 wt%) the plastic deformation disappears, the compression strength increases, contraction decreases, and the destruction of template goes through formation of Chernov-Luders Diagonal; but at the same time usage of high concentrations of the BP leads to increase of swelling of the polymer. The obtained results show that particles of brick powder able to significantly strengthen and structurize the EP-composite, at the same time make it more susceptible for liquid corrosion.

Keywords Epoxypolymer, Brick Powder, Strength, Compression, Moving, Tearing, Shrinkage, Swelling, Concentr.HNO₃, Life-Time, Durability

1. Introduction

Due to rising prices on polymeric raw materials, a perspectives of low-cost fillers became actual. In particular, it becomes relevant, if necessary fillers made of materials that pollute the environment (build, industrial and polymer waste), in relation to new ecologic initiatives in EC and US. One of their materials is brick powder.

Note that the question of hardening epoxy by filling alumina and silica fillers are still relevant, as evidenced the list of works[1-7]. For example, typical filler in studies of new EP-composites stands montmorillonite[3, 8], alumina[10], waste-glass[9]. But in literature data about filling of EP by brick powder have not detected.

The red brick is a product of hard thermo-treatment (>1000 °C) of aluminosilicates. The brick powder (BP) is a available product and perspective material as recycling filler for polymers. BP is well compatible with epoxyresins. In this work the character of BP-influence on strength and swelling of epoxy-polymer (EP). In this work, we avoided the stages of special treatment of BP (organo-modification, ultrasound, endurance in solutions). In the future, we plan to extend the work involving special modifications methods. It is established that decantation in water of thick fraction of

brick powder let obtain the filler with good compatibility with epoxy-resins. The possibilities of new composite system epoxypolymer – brick powder were investigated in this work.

2. Main Body

2.1. Experimental Part

For obtaining of EP-composites, in epoxydian-resin ED-20 (Russian UfaKhimProm production, see formula) added 12.5 wt% of polyethylene-polyamine. After 5 min of mechanical homogenization, EP-composite was hardened at normal conditions during 3 days, after that t100 oC (2 hours) was carried out. For measurements of compression strength (press Louis Shopper), composition was poured in cylindrical forms (d=1 cm). From their forms, the cylindrical templates 141.2 cm. The strength to adhesion moving (and tearing) detected on stall plates (and cylinders) adhesive area with glued surface $S = 3 \text{ cm}^2$ (for tearing – 5 cm²) in machines L.Shopper and Armaveer. Abrasion was determined on the R120 sandpaper with a common passage through 1.5 m. The shrinkage was determined by the change in specimen length of template h=1.5 cm with a micrometer. Swelling measured by growing of mass of templates (lens-form d=10 mm, h(in center)=2mm) in conc.HNO₃ during 15 days. Swell degree q measured as Life-time of template in c.HNO₃ evaluated as a time (days) of transition fro solid to viscous (when cannot to VZVESIT) state.

* Corresponding author:

stard6@mail.ru (Dmitro L. Starokadomsky)

Published online at <http://journal.sapub.org/ajps>

Copyright © 2012 Scientific & Academic Publishing. All Rights Reserved

As filler, the separated (by decantation) brick powder from red usual brick (smooth and dense, production of firm TMM, Ukraine) was used. The decantation carried out by one-stage method: powder poured into a container with distilled water and left for 2 min after shaking poured into a container with distilled water and left after shaking for 2 min.. Then, suspension was separated from sediment, and dried at 100 oC. Surface area of obtained powder was $S \approx 9 \text{ m}^2/\text{g}$.

2.2. Results: Compression Strength

Diagrams of compression of investigated epoxypolymer identify their dependence on the concentration and type of BP. As is shown (Figure 1), the diagram of destruction at compression for unfilled EP (H-composite) have a well-known[10-12] classic shape. We have two limits (thresholds). The first - the yield stress y_1 (tensile strength, the threshold for plastic deformation, plasticity limit) reflect the plastic deformation, when template transform to barrel – well-known effect for plastics and metals[10, 11].

For investigated composites, the low dispersion of y_1 (2-4% instead usual 10-15%) is characteristic.

After reaching the yield point, epoxypolymer sample retains the ability to resist compression for quite some time.

An extended plateau on the diagram after the first threshold corresponds to plastic deformation with an almost constant resistance - "yield plateau"[11]. Note that this can be critical in practically important cases - those which require resistance to the final destruction, and deformation is allowed (in the manufacture of structures, self-leveling floors, furniture). In our case, after y_1 , tension resistance of the sample is stabilized and then continues to grow (Figure 1) to the second limit (threshold) of strength y_2 , sometimes referred as "ultimate state", stress of destruction[12], the tensile strength[11, p.23], the limit of tensile strength[12, c.50], the threshold of complete destruction, etc. The destruction of the sample is complete after the second threshold strength y_2 .

The unfilled polymer is characterized by noticeable fluctuations (serration) of curve deformation-tension, especially at the "yield plateau" AB between the first and second threshold y_1 and y_2 (Figure 1, for $C=0 \text{ wt\%}$). When you add a 1 wt% of BP the form of the diagram maintained similar to H-composite, but it smoothed and serration after y_1 on "yield plateau" disappears (Figure 1), and "yield plateau" is compressed. At 2 wt% of the BP type of the diagram is similar to 1 wt%, but significantly different from the diagram for the 0 wt% (Figure 1): yield area is compressed, and the hardening stage tapers section BC before the final destruction (the limit of destruction and the second threshold strength). At 5 wt%, the "yield plateau" is almost no visible growth of tension is terminated and the final destruction site becomes more clear and sharp (Figure 1). Thus, with $C > 5 \text{ wt\%}$ the relative deformation and decrease after the first threshold (yield stress y_1) faster the stage of hardening, and tensile strength of y_2 (second

threshold) increases. This suggests a gradual loss of plasticity and increasing of fragile and hardness with increasing of C, that gives an increase of strength (Table 1). Regular change in the form of diagrams and correlation $y \sim C$ (hardening with increasing of C) interrupted at 10 wt%. At this concentration, the diagrams of compression back to "imperfect" form, which is typical for the unfilled polymer (Figure 1) - with a gear and a significant yield plateau. This can be considered as an evidence of disordering (loosening, appearance of defects, etc.) of the structure at $C=10 \text{ wt\%}$. At $C=20 \text{ wt\%}$, form of the diagram is similar to the form for 2-5 wt%, although threshold points are poorly visible (Figure 1). This may indicate an improvement of load distribution in the composite (no "failures" and "teeth" on the diagram).

The diagram form changes radically at $C=50 \text{ wt\%}$ (Figure 1). The relative plastic deformation almost stops (no "yield plateau"). And final destruction y_2 (the limit of destruction) can be seen by steps gradually (in stages). At $C=50 \text{ wt\%}$ the fracture behaviour of the sample is specific. For $C=0 \text{ %}$ (unfilled polymer) and $1 \leq C \leq 20 \text{ wt\%}$, the destruction of two thresholds (across the barrel-stage and plastic deformation) is completed by cracking along the longitudinal line in a compressed (flattened) sample or dispersal parts of the sample (as in the case of 10 wt%). Destruction of the same composite with 50 wt% of the BP is clearly along the diagonal - to "Chernoff-Luders lines"[13], while its original form does not change. This behaviour suggests the formation of a composite with such a high filling of the new reinforced low-plastic structure compared with the lowest content. Perhaps there is a sharp (percolation) changes in the structure at $20 < C < 50 \text{ wt\%}$.

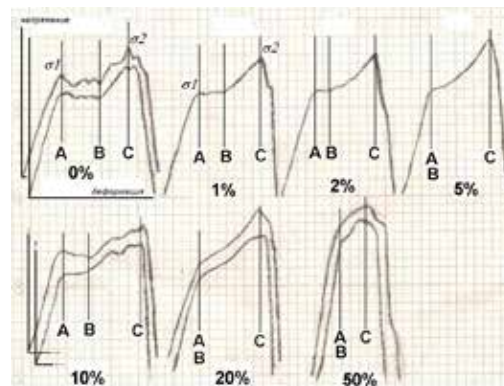


Figure 1. Diagrams of compression of epoxypolymer with 0-50% by weight of brick powder

It is interesting to consider the changes in the compressive strength of composites with increasing of filling (we accept the parameter $F = y \times 0.7$). After filling can increase not only average statistical, but the maximum values of F_1 (yield strength), and especially F_2 (tensile strength - the final destruction). Thus, for $C=5, 20$ and 50 wt\% , the value of $F_{2\text{max}}$ increases by 10% compared with $(F_{2\text{max}})_H$ and by 15-20% compared with averaged F_{2H} for unfilled polymer. This fact shows an essential reserve of composite strengthening by optimization the concentration

and the production technology of the composite. Note that the scatter of values (a difference of $F_{max} - F_{min}$) is very significant for the 0 and 10 wt%, to a lesser extent - for 5 and 20 wt%, but the minimum for $C=1, 2$ and 50 wt%. This may indicate completion of the optimum composite structuring under the effect of low and very high concentrations of BP, and confirms the assumption that the growth defect of the structure after 5% by mass and particularly in the vicinity of 10% of the mass of filling the BP. From Figure 3 it can be concluded that the most resistant to fracture under compression of the composite structure is formed around of 5 wt%, 20 wt% and especially 50 wt%.

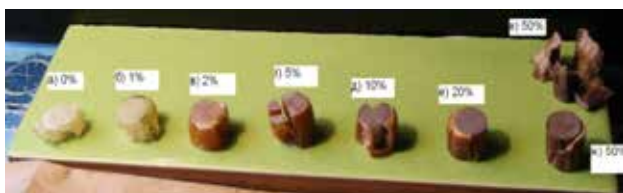


Figure 2. Compression failure types of the composite samples from 0 - 50 wt% of BP. Table 1. Compression strength for the first F_1 (plastic deformation) and the second F_2 (final failure) threshold destruction of epoxypolymer, depending on BP-content

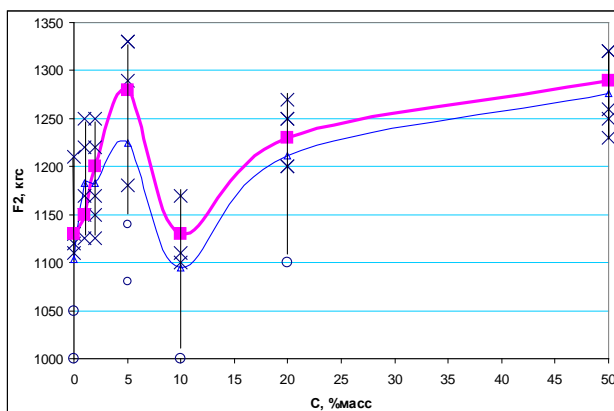


Figure 3. The dependence of the efforts for the second threshold F_2 of compressive strength (in kgf to 0.7 cm² of area) on the concentration of BP. Thick curve is averaging curve without the lowest values (only on cross-points, without marked by circles), thin - the curve of general average (of all points)

Strength of the composite curve of the concentration of BP in the resin is characterized by extremes. The introduction of small amounts of BP almost does not increase the strength of the composite F that distinguishes BP from aerosil-type nanosilicas. So, at $C=1$ wt% $F_1 \gg F_{1H}$ and F_2 grows only on 2-3%; at $C=2$ wt% $F_1 \gg F_{1H}$ and F_2 grows more noticeable (6%). Thus, for the 1-2 wt%, significant changes in the values of F_1 (limit of plasticity) is not observed, and weak strengthening of F_2 (the limit of destruction) takes place.

The same subtle influence of small amount of BP is observed for resistance to abrasion and shrinkage (see below, tab.2). Thus, despite the significant visual change in the composite (darkening Figure 2), no significant changes (deteriorating) in the strength characteristics of the composite, which can be used, for example, as decorative compositions). This can be called a significant difference BP

- microfiller from nanofillers (eg Aerosil), which gives a noticeable mechanical effect at low concentrations.

Increasing concentrations of BP up to 5 wt% gives obvious signs of composite hardening, especially $F_2 \gg F_{2H}$ (Table 1). It means non-randomness, hardly noticeable increases in the strength characteristics for the resin filled by small amount of alumina.

At 10 wt% character of destruction at compression changes and parameters of F_1 and F_2 falls to the level of H-composite. In this case because of the composite fragility it was difficult to fix the exact values of F_2 : every third test, the sample is not formed a barrel (as at other concentrations BP), and fly to pieces after the pass the first strength threshold F_1 . In some cases, filling with 10 wt% BP significantly increases the instability of instrument reading ("pointer jumping") when tested in compression, which is characteristic of the composite with highly-defective structure. Note that in research of composites "EP-nanosilica" the "loosening filler concentrations" also were found, when the strength parameters were decreased to a minimum (3 and 7 wt% of silica A-100) due to embrittlement of the polymer [6, 9]. However, this is not evidence of the fall of all strength parameters. For example, when $C = 10$ wt% were increased abrasion resistance (an increase of 15-20%) and the strength of adhesive tearing Θ (an increase in 1.5 times) compared with rates for H-composite (tab.2). Note that if compare 5 wt% to 10 wt% was no increase of swelling in a solution of HNO_3 (see below), i.e. embrittlement and estimated growth of the defect structure is not accompanied by changes in permeability (density) of polymer network.

In case of $C_{BP} \geq 20$ wt%, the new increase in compressive strength observes (growth rates F_1 and F_2 , Table 1). Figure 2 shows that the character of destruction is changed in comparison with 5-10 wt% content - it is similar to destruction for low-filled composites (1-2 wt%). For $C=20$ wt%, a small dispersion of the data - 2-3% (it is typical for $1 < C < 2$ wt%) observes. This suggests that at 20% by weight of the composite structure is optimized by eliminating or compensating for the typical for 10% of the mass defect of provoking increased fragility and instability properties.

With increasing of BP content up to 50 wt%, the tendency toward hardening of the composite reinforced (Table 1). The nature of fracture under compression changes significantly - it becomes a non-plastics. As you can see from Figure 1, it is almost impossible to distinguish the first threshold F_1 (the yield stress or plasticity) with such content, as a straight section of the curve 0-A of destruction extended (section AB disappears) and extended almost to the limit of final destruction F_2 (i.e. section BC is greatly reduced, Figure 1). But rough estimates of the values of F_1 (point A on the curve for the 50 wt%, Figure 1) suggest a very significant increase in their (up to 18-24%) compared to F_1 to H. There is also the maximum growth of value F_2 - over 14% (Table 1). Obviously, there is essential change in the structure of the composite, causing percolation phenomena while transition from $C=20$ to $C=50$ wt%.

Table 1. Compression strength for the first F1 (plastic deformation) and the second F2 (final failure) threshold destruction of epoxypolymer, depending on BP-content

	The values of the breaking load, kgf for the first and second thresholds compressive strength - F1 - F2 ($F = y \times 0.7$,MPa).				
Sample, wt% of BP	Averaged	Δ +-%	In % to FH	The maximum	In % to (Fmax)H
0 (H-composite)	95-113	5-7	100-100	99*-121	100 - 100
1 (K1)	95-115	2-3	100-102	95-115	96 - 95
2 (K2)	94-120	0-3	99-106	94-125	95 – 103
5 (K5)	97,5-128	3-7	103-113,5	102-133	103-110
10 (K10)	93,5-113	4-4	98-100	97-117	98 – 97
20 (K20)	100-123	2-3	105-109	100-127	101 – 105
50 (K50)	115 - 129	2-3	121 - 114	120*-132	121 - 110

* - The value of F1 is approximate

Table 2. Abrasion, adhesion strength to a shift in the separation and shrinkage of epoxy composites, depending on the content of the BP

		BP, wt%						
	D_{+-}	0	1	2	5	10	20	50
Abrasion D, mg	2	32		32		27	27	23
Separation $\Theta \times 5$, MPa	5	40	40		30	60		
Shift $t \times 3$, MPa	0,7	15		13,5				15
Shrinkage, mm	0,2	4	4	4	3,5	3,5	2	0,1

2.3. Other Characteristics of the Composites

Other mechanical characteristics also serve as indicators of structural change with the introduction of brick powder. Data on the shrinkage of the composites show a significant decrease only at high contents of BP. As can be seen from tab.2 at $C \leq 20$ wt% change of shrinkage is insignificant (about 10% compared with H-composite, tab.2). However, at 20 wt% is observed double reduction of shrinkage, and at 50 wt%, it almost does not occur (in 40 times less than for H-composite, tab.2). This confirms the conclusion of the hardening of the composite structure the high contents of BP.

Abrasion D (wear resistance) of composites does not change up to $C=10$ wt%. At $10 < C < 20$ wt% abrasion resistance is essential enhanced ($D < D_H$ by 15-20%, tab.2). This may be due to the emergence of a appearance of own Al_2O_3 - SiO_2 -structures in the polymer, which themselves have abrasive properties. This assumption is supported by a noticeable increase in wear resistance at a concentration of 50 wt% of the BP, when the wear is reduced by 40% compared with the H (tab.2). From tab.2 can see that by varying of C_{BP} can to increase the strength to adhesion separation (if $C = 10$ wt% , tab.2).

2.4. Effect of BP Filling on the Swelling of Polyepoxides

In the same time, filling changes (weaken) the resistance to decrease swelling in aggressive solutions, for example, in 20% HNO_3 . For low-filled composites ($C_{BP} = 1 - 2$ wt%) increase in swelling is not always apparent, for highly-filled

influence of alumina becomes significant. The weakening of the composite resistance to swelling at high contents of BP may be explained by high-permeability (channel, porous, etc.) structure in the polymer.

T In earlier our work was showed that a stage of quasi-saturation of polyepoxides swelling in dilute nitric acid[9] is possible. As you can see in 20% HNO_3 (Figure4), for unfilled polyepoxide (H-composite) and for $C=1$ wt% quasi-saturation is observed for 20-35 and 5-20 days of exposure; then begins a new stage of activation of swelling. For H, the swelling can be considered relatively small - 2.5% after 1 month, 4% after 2 months (Figure4).

Filling by $C > 1$ wt% leads to the disappearance of quasi-saturation site. In most cases, swelling curve can be divided into the initial stage of swelling area at high speed (up to 20 days), and subsequent swelling of the stage, where the rate is reduced (after which the effective rate of swelling decreases, Figure 4). For example, for $C=50$ wt% first stage of swelling (up to 20 days) is characterized by the rate of $V = 4$ %/day, while the second $V = 1,5$ %/day (Figure4).

Usually there is a clear regularity - with increasing of C the degree of swelling increases (Figure4, Figure5). For $C=1$ wt%, the nature of the swelling does not change: the curve "q-time" copies the curve for H-composite (Figure 4). However, at $C=2$ wt% and 5 wt%, there is intensification of swelling at all stages of aging.

For $C=10$ wt% the degree of swelling may sometimes decrease compared to 5% by mass (for example, with 7 days

exposure, Figure 5). This suggests that the structure of the composite at 5 and 10 wt% is about the same, which is expressed in the same permeability to molecules of the liquid medium. However, this conclusion seems surprising, given the dramatic differences in compressive strength (tab. 1, Figure 3) and separation (tab.2). We can suggest that in the range 5wt% a strong set, but more permeable to the solvent structure of the composite (relative to unfilled polymer). Most likely, a major role in structuring the composite play aluminosilicate framework structures. Thus, with increasing of filling of C=5 or 10 wt%, the density of the structure remains unchanged, but increases its imperfection and fragility, which leads to a drop in strength while maintaining resistance to swelling (compared to 5 wt%).

The noticeable intensification of swelling occur for $C_{BP}=20$ wt% and especially 50 wt% (Figure4, Figure5). At 20 wt%, the swelling increased very significantly ($q(20\text{wt\%})/q(H) \gg 3$, $q(20\text{wt\%})/q(5 \text{ or } 10\text{wt\%}) \gg 2$). This suggests a significant loosening of the structure of composite from C=10 to C=20 wt%, which is typical for nanosilica[9]. Trends to increase swelling with increasing of filling continues from 20 to 50 wt%. For C=50 wt% can see the visual differences: the composite is similar to cast stone, but when exposed to a solution of HNO_3 , its quickly brightens. The growth of strength at 20 and especially 50wt% shows a high-permeability formation for liquids, but resistant to the stresses of the composite frame structure.

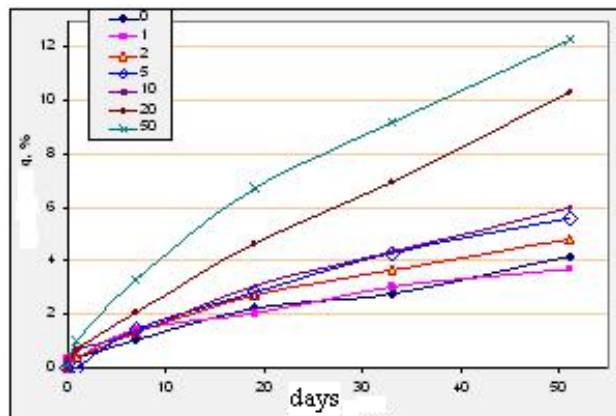


Figure 4. The swelling curves of PE with 0-50 wt% of BP in 20% HNO_3

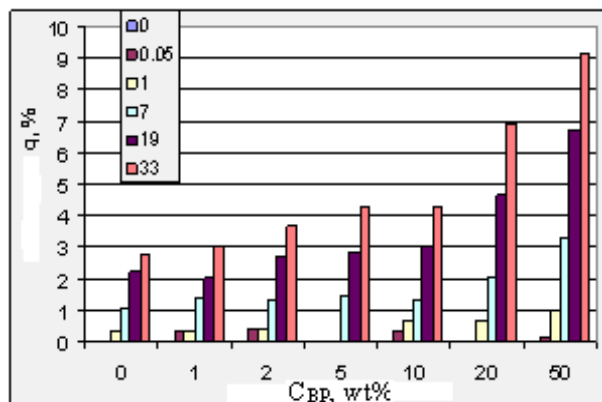


Figure 5. Changes in the degree of swelling of PE with 0-50 wt% of BP as a function of exposure time in 20% HNO_3

3. Conclusions

The introduction of BP in a wide concentration range (1-50 wt%) can be an effective method to control the strength, shrinkage and durability/swelling of epoxypolymer composite.

Each concentration of BP-filler is characterized by own structure of compression diagram. The introduction of BP generally has a reinforcing, structuring effect on the epoxypolymer. Also established the possibility of the existence of not only optimal, but suboptimal concentrations of BP (10 wt%) composites, in which the inherent instability and loss of original strength properties takes place.

It is shown that low concentrations of BP (1-2 wt%) have weak effect on compressive strength, abrasive, swelling and shrinkage of the composite. The introduction of BP in large quantities can prevent shrinkage of the composites, and in this case - to increase the compressive strength and abrasion resistance of composites. In this case, however, starting with $C_{BP}=2$ wt% resistance of the composite to an aggressive (acidic) environment is reduced. This is reflected in the growth of the swelling in the nitric acid of filling is increased, especially after $C_{BP}=10$ wt%.

The effect of significant changes in the properties of the composite (percolation threshold) in $C_{BP}=50\%$, which influences in a change in the form of diagrams, the nature of fracture, and a sharp rise in the compressive strength, abrasion, swelling and reducing shrinkage.

REFERENCES

- [1] M.Worzakowska. "Epoxy matrix composites filled with glass wastes." , in Proceedings of Intern.Conf. "Actual Problems of Surface Chemistry", Kiev, Ukraine, 2010.
- [2] V.L. Demchenko, V. I. Shtompel, V.O. Vilensky, "Features of the structure of composites based on polymer mesh structure and oxides of Fe (III) and Al (III), formed in a constant electric field", Polymer Journal (in Russian), V.31, № 3, pp.235-243, 2009.
- [3] Y.Y.Choi, S.H.Lee, S.H.Ryu, "Effect of silane functionalization of montmorillonite on epoxy/montmorillonite nanocomposite", Polymer Bulletin, N 63, pp.47-55, 2009.
- [4] "Polymer/layered silicate nanocomposites by combined intercalative polymerisation and melt intercalation: a masterbatch process", B.Lepoittevin, N.Pantoustiera, M.Devaickenaerea, M.Alexandrea, C.Callergb, R.Jeromeb, C.Henristd, A.Rulmond, Ph.Dubois, POLYMER, V.44, N7, pp.2033-2040, 2003.
- [5] I.G. Dobrotvor, P.D. Stuhlyak, A.V. Buketov, "Determination of optimal ranges of dispersed filler content in epoxypolymer composition", Phys.-Chim.Mehanika Materials (Riga, EC), № 6, ppp.32-39, 2009.
- [6] D.L. Starokadomsky, "The effect of the content of the unmodified nanodispersed silica with different specific surface on the mechanical properties of epoxypolymer

- composites”, Journal of Applied Chemistry, № 12, pp.2045-2051, 2008.
- [7] V.A. Liopo, V.A. Struk, S. Avdeychik, “The mechanism of the doping nanoscale modifiers in the polymer matrix”, Plastics, 2007, № 8, pp..36-39.
- [8] V.A. Borisov, Y.U. Bedanokov, A.M. Karmok, A.K. Mikitaev, M.A. Mikitaev, E.R. Turaev, “Properties of polymer nanocomposites based on organo-modified Na +-montmorillonite”, Plastics, 2007, № 7, pp.30-32.
- [9] D.L. Starokadomsky, “The concentration and dispersity of aerosil as a factor of change in chemical resistance and durability of epoxy-based DE-20 + PEPA”, Proceedings Slavpolykom 2008, Kiev-Yalta, 2008, pp.40-44.
- [10] Epoxy or polyepoxide containing coating..Composition comprising thermosetting plastic resin with comminuted recycled glass powder as a filler. // Patents In Field 427/386 - patents.justia.com/field/427-386.html.
- [11] M.M.Fylonenko-Borodin, S.M. Yzyumov, B.A. Olysov, I.N. Kudryavtsev, L.I. Malginov, “Course of resistance of materials”, Moscow: USSR-HYTTL, 1956, 650 p.
- [12] NK Snytko, “Resistance of materials”, Leningrad: Edition LHU, 1975, 370 p.
- [13] Introduction to resistance of materials. Ed. VE Melnikov, St.-Petersburg (Russia), 1999, 160 p.
- [14] Stepin PA, “Resistance of materials”, Moscow, 1998, 320 p