

# Analysis of Temperature Changes during Dry Drilling of Austenitic Stainless Steels on Twist Drills Having Different Point Angles

Jolene S. Vas<sup>1,\*</sup>, Aster Fernandes<sup>1</sup>, Arnold D'Souza<sup>1</sup>, Ankith Rai<sup>1</sup>, Jaimon D. Quadros<sup>2</sup>

<sup>1</sup>UG Students, Department of Mechanical Engineering, Sahyadri College of Engineering & Management, Mangalore, India

<sup>2</sup>Department of Mechanical Engineering, Birla Institute of Technology, Offshore campus, Ras-Al-Khaimah, UAE

**Abstract** In this work, effects of drilling parameters (feed rate and spindle speed) on the twist drill bit temperature in drilling of austenitic stainless steel material with and without the use of coolant is experimentally investigated. During drilling experiments, the drill bit temperature was measured by using SMART SENSOR AR360 Infrared Thermometer. The performance parameters viz. feed rate and spindle speed are varied as per  $L_9$  orthogonal array. The experiments were conducted by using High Speed Steel (HSS) drills having 82°, 100° and 118° drill point angles respectively. Analysis of temperature on the drilling parameters concluded that, the drilling temperature of the specimen increases with increase in both cutting speed and feed rate. This work thoroughly construes that 118° drill point angle produced the highest drilling temperature during the specimen drilling. Thus in order to reduce the thermal effects during machining of the specimen, the 80° drill point angle is recommended.

**Keywords** Drilling, Austenitic stainless steel, Cutting speed, Feed rate, High Speed Steel

## 1. Introduction

The cutting temperature directly influences the hole sensitivity (hole diameter, perpendicularity, and cylindricity), surface roughness, and tool wear. The experimental and numerical investigation of the temperature changes that occur on the cutting tool during the material removal processes is a traditional concern. In the aerospace industry depending on the application, hole quality is very important. Thus the quality characteristics of holes in this experimental investigation process are analyzed using spindle speed, feed rate and different drill diameter are as input parameter.

During the drilling process, the most important factor affecting the cutting tool performance and work-piece properties is the cutting temperature that emerges between the drill bit and chip. The cutting temperature directly influences the hole sensitivity (hole diameter, perpendicularity, and cylindricity), surface roughness, and tool wear. The experimental and numerical investigation of the temperature changes have been recently conducted in works to calculate the cutting temperature by using FEM have also been conducted. Chen [1] has developed the 3-D finite element model to be able to compute the temperature

distribution that may take place at the first cutting edge of the drilling tool and along the flank face. Fuh et al. [2] calculated the temperature distribution on the conventional drill during the cutting process by means of 3-D FEM. In this study, the effects of the cutting depth, cutting speed, web thickness, and helix angle on the temperature changes are investigated. Agapiou and Devires [3, 4] have analytically calculated the temperature distribution of twist drills on the flank face and cutting edge to explain thermal phenomena during the cutting process. They also have proposed a comparison between experimental and analytical results. On the other hand, Agapiou and Stephenson [5] have described a model for calculating transient and steady-state drill temperatures for a drill with arbitrary geometries. They have additionally compared the analytical results acquired to the experimental ones gathered by implementing welded thermocouple and thin wire thermo-junction methods. Despite that there are many experimental works on turning and grinding operations in the literature, there is little work directed toward calculating the drill temperature. Bono et al. [6, 7] developed a model for predicting the heat flow into the work-piece and investigated the influence of the heat that emerges on hole diameter and cylindricity in dry drilling. Finally, he has presented a comparison between numerical and experimental results. Bağcı [8] has developed a new approach for experimental measurement of the drill bit temperature in the dry drilling process. Drill temperatures were measured by inserting standard thermocouples through

\* Corresponding author:

jaimonq@gmail.com (Jolene S. Vas)

Published online at <http://journal.sapub.org/jmea>

Copyright © 2016 Scientific & Academic Publishing. All Rights Reserved

the coolant (oil) hole of TiAlN-coated carbide drills. In his work, the effects of sequential, continuous, and step by step dry drilling operations and drilling parameters on the drill bit temperature experimentally and numerically have been investigated. The drill bit temperature was predicted using a numerical computation with Third Wave Advant Edge FEM software based on langrangian explicit method. Finally, he has presented a comparison between experimental study and finite element analyses (FEA). Kalidas *et al.* [9] has measured the work-piece temperature to find out how different drill coatings affects the hole quality under dry and wet cutting conditions. For this purpose, four thermocouples were inserted onto the work-piece and the temperature values for various feed rates and spindle speeds were determined. V. N. Gaitonde *et al.* [10] used Taguchi L9 Methodology to design the number of experiments for drilling of AISI 316L by varying the input parameters cutting speed, point angle, lip angle and found that point angle has major influence on burr height. Tsann-Rong Lin *et al.* [11] studied the Cutting behavior of a TiN-coated carbide drill with curved cutting edges during the high speed machining of stainless steel AISI304 and measured surface roughness and burr height. Based on the literature cited above, the current research endeavour is one such attempt to determine the temperature for drill bits of drill point angles 82°, 100° and 118°.

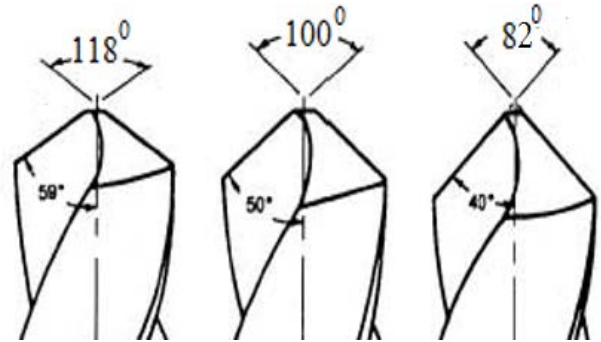
## 2. Materials

The material used for drilling in the present study is Austenitic Stainless Steel. These are alloys containing chromium and nickel, and sometimes molybdenum and nitrogen, structured around composition of iron, 18% chromium, and 8% nickel. Austenitic stainless steels replace the majority of their nickel content with manganese to reduce cost. Austenitic steels are not hardenable by heat treatment. This alloy exhibits superior resistance to stress-corrosion cracking in boiling 20-40% sulphuric acid. It has excellent mechanical properties and the presence of Niobium in the alloy minimizes the precipitation of carbides during welding.

## 3. Plan of Experiments

Taguchi method uses a special design of orthogonal arrays to study the entire parameter space with only a small number of experiments. Taguchi is the developer of the Taguchi method [12]. Taguchi methods(orthogonal array) has been widely utilized in engineering analysis and consists of a plan of experiments with the objective of acquiring data in a controlled way, in order to obtain information about the behavior of a given process. Taguchi methods, which combine the experiment design theory and the quality loss function concept, have been used in developing robust designs of products and processes and in solving some confusing problems of manufacturing [13]. The orthogonal

array selected was the L<sub>9</sub> (24) which has nine rows corresponding to the number of tests(eight degrees of freedom) with two columns at three levels, as shown in Table 1.



**Figure 1.** Drill point angles of different drill point geometries used in the present study

**Table 1.** Orthogonal array L<sub>9</sub> of Taguchi with factors at different levels

Experimental Runs	Cutting Speed (RPM)	Feed Rate (mm/min)
1	600	30
2	600	45
3	600	60
4	700	30
5	700	45
6	700	60
7	800	30
8	800	45
9	800	60

## 4. Machining Set-up and Drilling Procedure

Drilling was performed on a BATLIBOI make radial drilling machine by using HSS twist drill of 12 mm diameter with 82°, 100° and 118° point angles shown in Figure 1. The temperature was recorded for different cutting conditions by using SMART SENSOR AR360 Infrared Thermometer which is a non- contact digital thermometer providing temperature readings ranging from -50°C to 320°C with an accuracy of ±2%. Drilling operations were carried out on the austenitic steel plates with the cutting conditions that are already listed. The experimental set up is shown in Figure 2. The coolant ECOCUT SSN 322 neat oil with 40.2 cSi at 40°C from FUCHS was used as MQL oil for thin pulsed jet system.

## 5. Results and Discussions

The Figures below shows the detailed drilling temperature response values obtained with respect to feed rate and cutting

speed respectively with and without the use of coolant. It is observed from Figure 3 (a, b) that, drilling temperature is found to increase considerably with the increase in feed rate for drill point angles of 82° and 100°. However for drill point angle of 118°, temperature tends to marginally decrease with increasing feed rate. Thus it can be thoroughly construed that, temperature changes produced by drill point angle of 118° have a comparatively lesser effect in drilling austenitic stainless steels when compared to 82° and 100° drill point angles. From previous studies [13, 14] it has already been concluded that thrust force and torque generally increase with increase in feed rate. This was mainly due to the increase in the cross-sectional area of the un-deformed chip. This increases the hardness and the cutting resistance of the material resulting in wears the cutting edges of the drill through drilling one hole. Thus during penetration of the drill bit into the material, the un-deformed chip tends to melt due

to increased friction at the tool-chip interface likewise increasing the temperature. It is observed from Figures 4 (a, b) that, drilling temperature is found to increase considerably with the increase in cutting speed for all drill point angles of 82°, 100° and 118° respectively. Unlike drilling with respect to feed rate; the drilling temperature for increase in cutting speed showed sizable deviation for all the drill point angles employed in the present study. During drilling of austenitic steel specimens, drilling torque increases with the increase in RPM of the spindle and this torque increases with the increase in depth of cut. This developing torque enhances the plastic deformation over the sides of the drill bit resulting in rigorous chip formation and larger burr formation. The temperature changes observed during the use of coolant were much lesser when compared to drilling without its use.

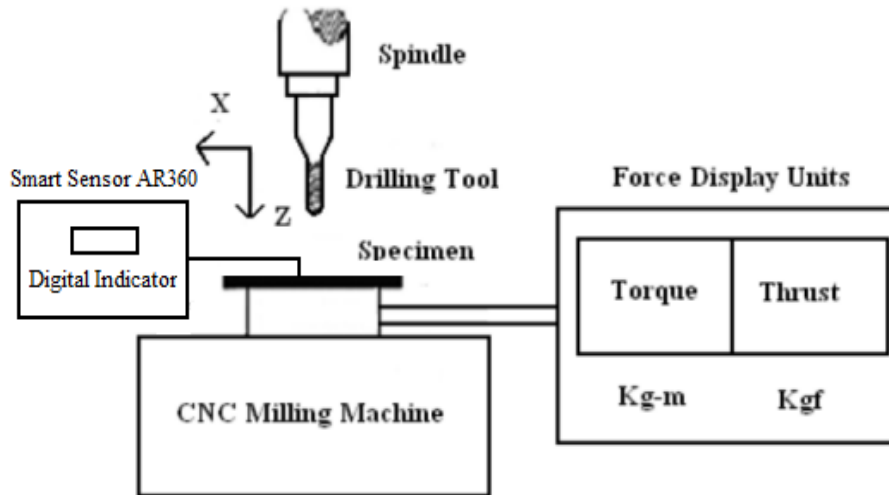


Figure 2. Experimental Set up

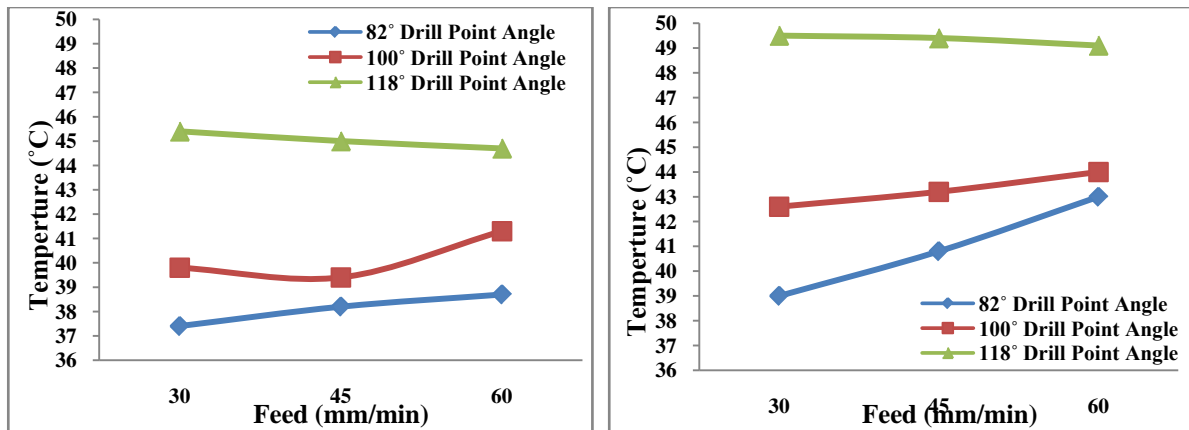
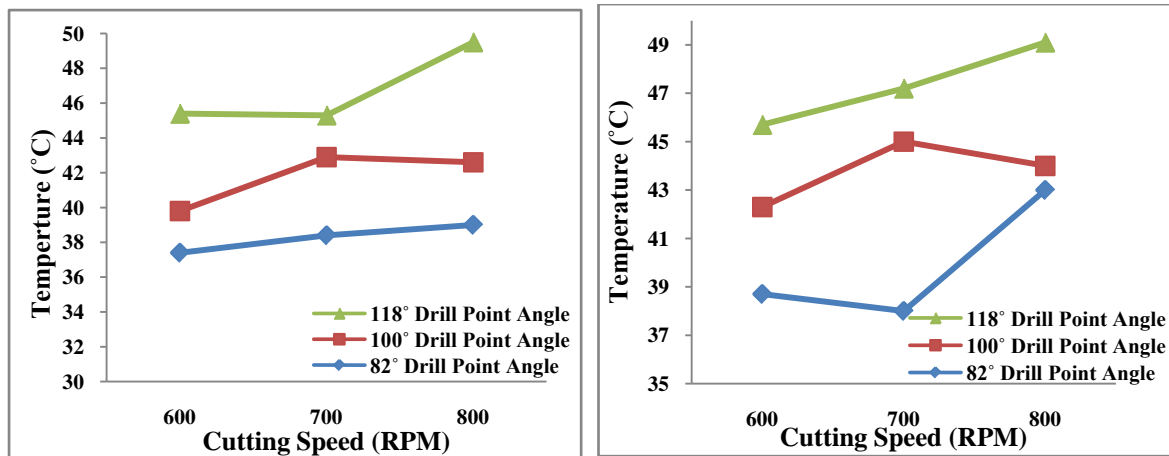
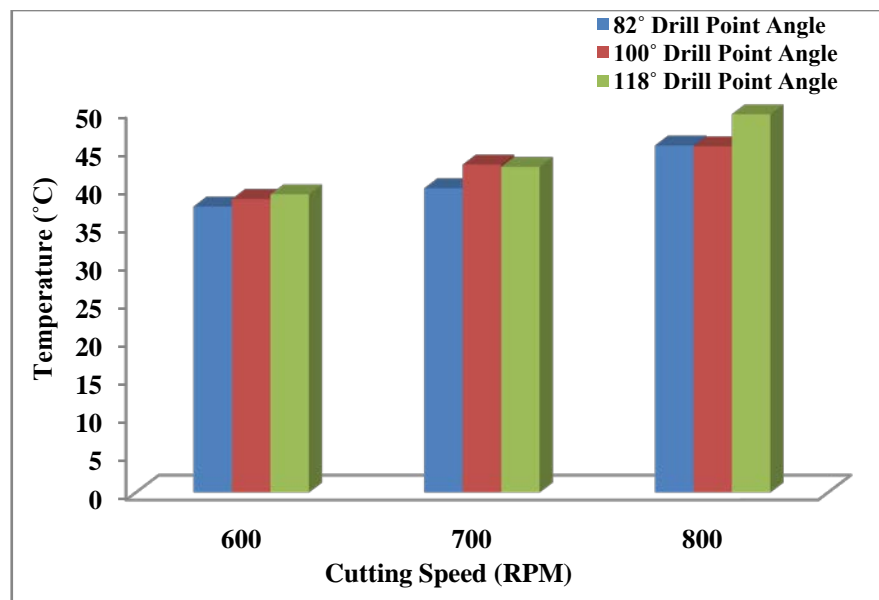


Figure 3. Variation of drilling Temperature (°C) with respect to Feed (mm/min) for drill point angles of 82°, 100° and 118° respectively. (a) With coolant; (b) Without coolant



**Figure 4.** Variation of drilling Temperature (°C) with respect to Cutting Speed (RPM) for drill point angles of 82°, 100° and 118° respectively. (a) With coolant; (b) Without coolant



**Figure 5.** Variation of drill temperature for different drill point angles

This chip formation in turn leads to accumulation of large amount of chip at the tool-chip interface. This causes plastic deformation thus inducing a high temperature rise which results in larger burrs. During the drilling process, 90% of work is converted to heat as a result of the plastic deformation [15]. This temperature affects a specific region of the chip, tools and work-piece. When machining low alloy steels, the tool reaching a high temperature wears quickly because of the high cutting temperature and a strong adhesion between the tool and the work-piece; and the high stresses developed at the cutting edge of the tool may cause a plastic deformation and accelerate the tool wear [16]. The trend in Figure 5 shows that the for various drill point angles the bar graph reveals that as the drill point increases, the drilling temperature value increases i.e. 80° point angle drill produced the least drilling temperature and 118° point angle drill produces the highest drilling temperature. The plausible reason for this could be the surface area in contact with the tool-chip interface. The 82° drill point angle has a pointed

geometry and therefore emphasizes on thrust force producing less friction at the tool-chip interface thus generating lesser temperature during drilling of the specimen. However in case of an 118° drill point angle, the larger surface area around the drill point, tends to produce more friction at the tool-chip interface thus generating a higher temperature at the tool-chip interface during drilling of the specimen.

## 6. Conclusions

The present work analyses the effects of drilling parameters viz. feed rate and spindle speed on the twist drill bit temperature in the dry drilling of austenitic stainless steel material. The following conclusions have been drawn:

- The drilling temperature of the specimen is found to increase with the increase in feed rate for all the drill point angles employed in the study.

- The drilling temperature is found to increase considerably with the increase in cutting speed for all drill point angles.
- The 80° point angle drill recorded the least drilling temperature and 118° point angle drill recorded the highest drilling temperature during drilling of austenitic steel specimens.
- This work thoroughly construes that 118° drill point angle produced the highest drilling temperature during the specimen drilling. Thus in order to reduce the thermal effects during machining of the specimen, the 80° drill point angle is recommended.

---

## REFERENCES

- [1] Chen, W., 1996, Effect of the cross-sectional shape design of a drill body on drill temperature distributions, *International Communications of Heat and Mass Transfer*, 23(3), 355–366.
- [2] Fuh, K., Liang, W. C., 1994, Temperature rise in twist drills with a finite element approach, *International Communications of Heat and Mass Transfer*, 21(3), 345–358.
- [3] Agapiou, J. S., DeVries, M. F., 1990, On the determination of thermal phenomena during a drilling process – part I, analytical models of twist drill temperature distributions, *International Journal of Machine Tools and Manufacturing*, 30(2), 203–215.
- [4] Agapiou, J. S., DeVries, M. F., 1990, On the determination of thermal phenomena during a drilling process – part II, comparison of experimental and analytical twist drill temperature distributions, *International Journal of Machine Tools and Manufacturing*, 30(2), 217–226.
- [5] Agapiou, J. S., Stephenson, D. A., 1994, Analytical and experimental studies of drill temperatures, *Journal of Industrial Engineering*, 116(1), 54–60.
- [6] Bono M, Ni J., 2002, A method for measuring the temperature distribution along the cutting edges of a drill, *Journal of Manufacturing Science and Engineering*, 124(4), 921–923.
- [7] Bono, M., Ni, J., 2001, The effects of thermal distortions on the diameter and cylindricity of dry drilled holes, *International Journal of Machine Tools and Manufacturing*, 41(5), 2261–2270.
- [8] Bağcı, E., 2004, Modelling of high speed machining processes for prediction tool forces, stresses and temperatures using FEM simulation. Thesis Dissertation, Gebze Institute of Technology, Gebze-Kocaeli, Turkey, (in Turkish).
- [9] Kalidas, S., DeVor, R. E., Kapoor, S. G., 2001, Experimental investigation of the effect of drill coatings on hole quality under dry and wet drilling conditions, *Surface Coatings Technology*, 148(2-3), 117–128.
- [10] Gaitone, V. N., Karnik, S. R., Achyuth, B. T., Siddeswarappa, B., 2008, Taguchi optimization in drilling of AISI 316L stainless steel to minimize burr size using multi-performance objective based on membership function, *Journal of materials processing technology*, 202(1-3), 374–379.
- [11] Tsann-Rong, L., 2002, Cutting behavior of a TiN-coated carbide drill with curved cutting edges during the high-speed machining of stainless steel, *Journal of Materials Processing Technology*, 127(1), 8–16.
- [12] Taguchi, G., 1990, Introduction to quality engineering. Asian Productivity Organization, Tokyo.
- [13] Tsao, C. C., Hocheng, H., 2004, Taguchi analysis of delamination associated with various drill bits in drilling of composite material, *International Journal of Machine Tools and Manufacturing*, 44(10), 1085–1090.
- [14] Raju, B. R., Suresha, B., Swamy, R. P., Swamy, B., Kanthraju, G., 2013, Assessment of Cutting Parameters Influencing on Thrust Force and Torque during Drilling Particulate Filled Glass Fabric Reinforced Epoxy Composites, *Journal of Minerals and Materials Characterization and Engineering*, 1(3), 101–109.
- [15] Ezugwu, E. Q., 1997, Titanium alloys and their machinability – a review, *Journal of Materials Processing Technology*, 68(3), 262–274.
- [16] Dearnley, D. A., Gearson, A. N., 1986, Evaluation of principal wear mechanisms of cemented carbides and ceramics used for machining titanium alloy IMI 318, *Material Science and Technology*, 2(1), 47–58.