

Study the Precipitation of Sb in Pb Based Alloys Using Stress-Strain Characteristics and Positron Annihilation Technique

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Abstract The effect of Sb-content and strain rate ($\dot{\epsilon}$) on the work hardening characteristics of Pb-1.5wt% Sb alloys were studied by stress-strain measurements and positron annihilation lifetime spectroscopy (PALS). Annealing of the samples was made in the air for 2 hours at 423 ± 2 K and then they were quenched in water at room temperature (RT). The samples were stretched at $\dot{\epsilon}$ of 5.4×10^{-5} , 6.7×10^{-4} and $1.2 \times 10^{-3} \text{ s}^{-1}$ at RT up to fracture. It was found that, (i) at constant $\dot{\epsilon}$ increasing Sb-content, increases σ_F and work hardening coefficient χ_p while ϵ_f decreases (ii) for each alloy, σ_F and χ_p decreases with increasing $\dot{\epsilon}$ while ϵ_f increases (iii) with increasing Sb-content, the lifetime component τ_1 is nearly constant and its value is about 0.195 ns, which agrees with the positron lifetime in bulk Pb (0.198 ns). Also, τ_2 is invariable with a value about 0.288 ns (iv) the intensity I_1 decreases with increasing Sb-content while I_2 and the mean lifetime (τ_m) increase. The microstructure of Pb-Sb alloys were investigated using scanning electron microscope (SEM) and energy dispersive X-ray spectroscopy (EDS).

Keywords Positron annihilation, Pb-Sb alloy, Fracture stress, Strain rate

1. Introduction

Pb alloys have many applications in industry. They are the best stable materials for the production of battery grids in Pb-acid electric accumulators. The main alloying system used in these grids was Pb-Sb alloy. The addition of Sb strengthens and hardens the Pb grids for improved handling and casting, also it enhances the conductive properties [1-3]. Such enhancement in the mechanical properties is due to some significant segregation of Sb at grain boundaries and also to the increase in the concentration of the alloying vacancies which could modify the viscous flow processes along the grain boundaries [4].

Positron annihilation spectroscopy (PAS) can provide important information about the concentration, configuration and internal structure of the lattice defects in solids [5-8]. It has particular advantages compared to other traditional tools in resolving small vacancy clusters, voids, dislocation lines or loops, and jogs. Also, PAS was used deeply to study the precipitation kinetics in different alloys [9, 10] and to investigate the recovery stages and recrystallization processes [11, 12].

The thorough surveying of the literature has revealed that there are only three papers handled the topic of positron annihilation study in Pb based alloys. Menai et al. [13] studied positron annihilation in quenched and irradiated pure Pb and in quenched Pb (Ag) alloys. They found that, the precipitation of Ag atoms in dilute alloys should be understood in terms of Ag-Pb interstitially migrating pairs. The presence of di-interstitial (Ag-Ag) or complexes (Ag(s)-Vacancies) as mobile defects responsible for the Ag transport process in concentrated alloys. Belaidi et al. [14] investigated the defects and their diffusion, which induce grain boundary migration in a Pb-Sn system. Dorikens-Vanpraet et al. [15] determined the activation energy for the recovery of the dislocations in deformed Pb at liquid nitrogen temperature by PAS. Its value was found to be equal 0.43 ± 0.03 eV. As was noticed, little attention has been given to the topic of studying the effect of Sb-content on the work-hardening characteristics in Pb based alloy by PAS which represents a gap that has to be filled.

2. Experimental Procedures

Pb-1.5wt%Sb alloys were prepared from high purity Pb (99.99%) and Sb (99.99%) by melting a mixture of the appropriate weights under vacuum in a high purity graphite crucible, in a high frequency induction furnace. The obtained ingot was homogenized at 553 K for 4 hours, and then cold

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drawn into two forms, wires of diameter 0.6 mm and sheets of thickness 1 mm. Chemical analysis was made for the different samples as presented in Table (1). It is obvious that the alloy composition is very close to the required one. Annealing of the samples was made in the air for two hours at 423 ± 2 K then quenched in water at RT.

The tensile test was performed using a computerized locally made tensile testing machine. More details about this machine were already mentioned before [16]. The samples were stretched at different strain rates ($\dot{\epsilon}$) of 5.4×10^{-5} , 6.7×10^{-4} and $1.2 \times 10^{-3} \text{ s}^{-1}$ at RT up to fracture. The microstructure of Pb-Sb alloys was investigated using scanning electron microscope (SEM) (JEOL, JSM-5400). Prior to microscopic investigations, the samples were carefully cleaned, mechanically polished then electrochemically polished.

Table 1. Typical chemical analysis of Pb-1-5wt% Sb alloys

Alloy	Percent by weight	
	Pb	Sb
Pb-1wt% Sb	98.9	1.1
Pb-2wt% Sb	98.1	1.9
Pb-3wt% Sb	96.7	3.3
Pb-4wt% Sb	95.8	4.2
Pb-5wt% Sb	95.1	4.9

The positron annihilation lifetime spectroscopy (PALS) was performed using a conventional fast-fast coincidence system. A positron source (^{22}Na), sealed in a thin Kapton foil (7 μm thick), was mounted in a sample ($10 \times 10 \text{ mm}^2$ with a thickness of 1mm) –source–sample sandwich. The time resolution of the system was 240 ps (full width at half maximum, FWHM) with a time calibration of 53 ps/ch. The PAL spectra containing 1.5×10^6 counts were analyzed using LT 9.0 [17] program in terms of two lifetime components τ_1 and τ_2 with relative intensities I_1 and I_2 taking into consideration the source corrections which gives single lifetime component (0.368 ns) with intensity 16%. The variation in lifetime values is relevant to defect type, while changes in the intensities reflect the defect concentration. Positron mean lifetime, τ_m , can be calculated using the formula

$$\tau_m = \tau_1 I_1 + \tau_2 I_2 \quad (1)$$

3. Experimental Results and Observations

Typical engineering stress-strain curves of Pb-1-5wt % Sb alloys at different strain rates (5.4×10^{-5} , 6.7×10^{-4} and $1.2 \times 10^{-3} \text{ s}^{-1}$) are shown in Fig.(1). The levels of the stress–strain curves were found to be sensitive to the values of $\dot{\epsilon}$ and Sb-content. The maximum stress applied to the sample at the fracture point was taken as the fracture stress (σ_F) and the corresponding strain is the fracture strain (ϵ_F). The dependence of σ_F and ϵ_F on the Sb-content at different $\dot{\epsilon}$ is

shown in Figs. (2) and (3), respectively. From these figures, it is clear that, (i) at constant $\dot{\epsilon}$, with increasing Sb-content, σ_F increases while ϵ_F decreases (ii) for each alloy, σ_F decreases with increasing $\dot{\epsilon}$ while ϵ_F increases. The work-hardening coefficient, predicted by the Mott's model [18], is given by;

$$\chi_p = \left(\frac{\partial \sigma^2}{\partial \epsilon} \right)_T \quad (2)$$

χ_p was found from the parabolic part of the stress-strain curve, after the elastic part, by drawing the squared-value of stress σ with strain ϵ then calculating the slope of these straight lines. χ_p is related to the shear modulus, grain size and fatigue [19]. Figure (4) shows the dependence of χ_p on the Sb-content at different $\dot{\epsilon}$. It is obvious that χ_p increases as Sb-content increases while it decreases with increasing $\dot{\epsilon}$. Figure (5) shows the micrographs of two samples, Pb-1wt% Sb and Pb-5wt% Sb alloys, obtained by SEM. The pictures reveal the effect of Sb content on the microstructure of the samples. Such micrographs revealed two phases, one of them is dark while the other is white. The white phase was detected to be Sb-phase embedded in dark phase (Pb) and this was confirmed by EDS investigation

The variations of the lifetime components (τ_1 and τ_2) and their intensities (I_1 and I_2) with increasing Sb-content for Pb-1-5wt% Sb alloys are shown in Figs. (6 & 7). It is clear that, (i) the lifetime component τ_1 is nearly constant and its value is about 0.195 ns. Also, τ_2 is invariable with a value about 0.288 ns (ii) the intensity I_1 decreases with increasing Sb-content while I_2 increases. The mean lifetime τ_m as a function of Sb-content is shown in Fig. 8. It is clear that τ_m increases as Sb-content increases.

4. Discussions

It should be mentioned that, the engineering stress-strain curves were considered as raw experimental data in the present work. So, it is more appropriate to discuss the parameters extracted from these curves (σ_F , ϵ_F and χ_p) as shown in Figs (2-4). According to the phase diagram [20] of Pb-Sb system, Pb-1-5wt% Sb consists of two phases, namely α -solid solution (Pb-rich phase) and considerable amounts of β -phase (Sb-rich phase) formed at the boundaries of α -phase [3, 21]. Increasing the content of Sb in Pb based alloys leads to an increase in the hardness of the alloy. This is because Sb segregates at grain boundaries of Pb phase forming Sb-rich phase also there will be more interfaces between α and β phases which hinder the dislocation motion [4]. The SEM micrographs (Figure 5) indicate that there are more interfaces as Sb increases. These interfaces could modify the viscous flow processes along the grain boundaries which causes an increase in the alloy hardness, i.e, σ_F and χ_p increases, but ϵ_F decreases [22].

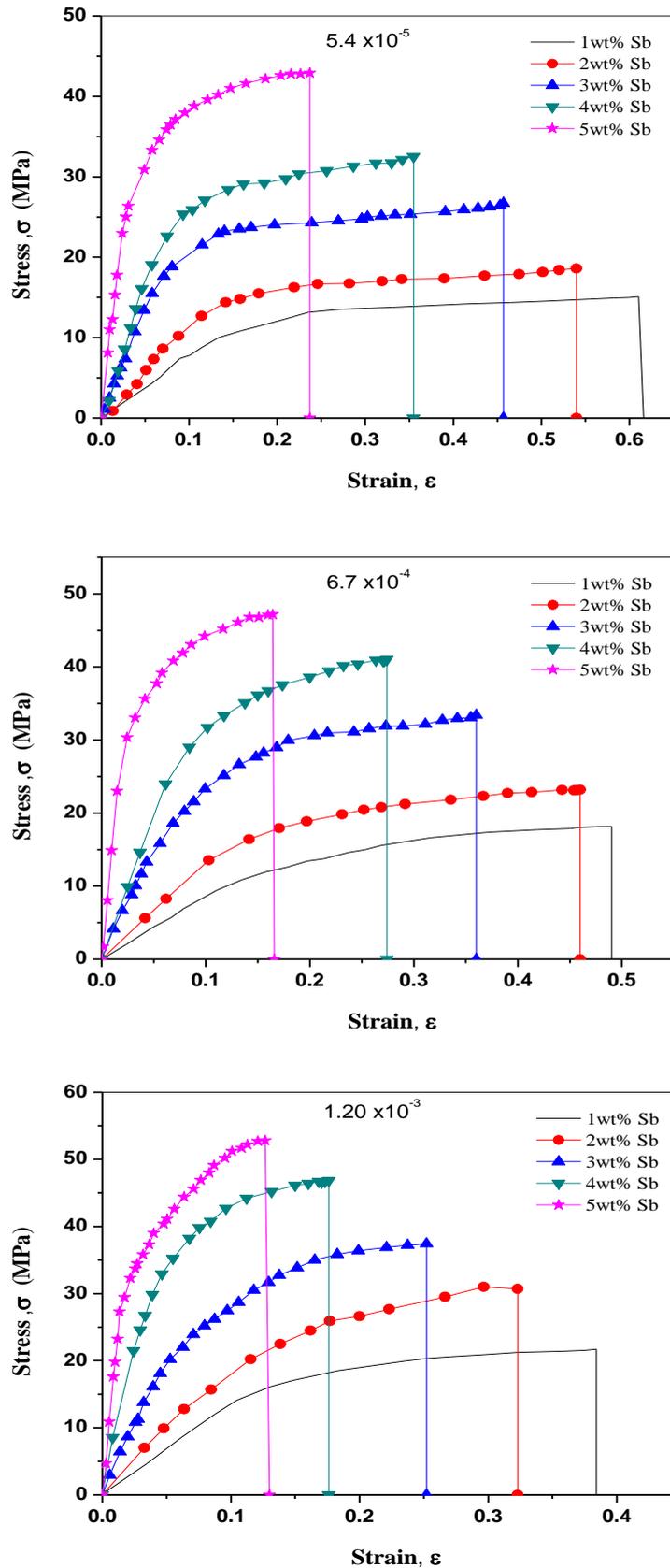


Figure 1. Stress-strain curves of Pb-1-5wt% Sb alloy at different strain rates (5.4×10^{-5} , 6.7×10^{-4} and 1.2×10^{-3} s $^{-1}$)

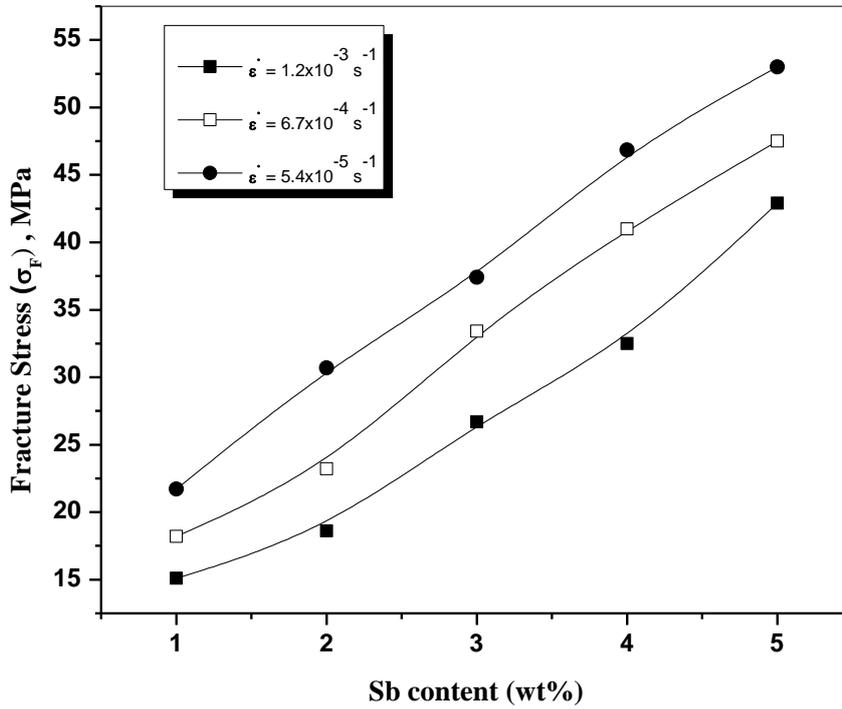


Figure 2. The dependence of fracture stress (σ_F) on the Sb-content at different strain rates (5.4×10^{-5} , 6.7×10^{-4} and $1.2 \times 10^{-3} \text{ s}^{-1}$)

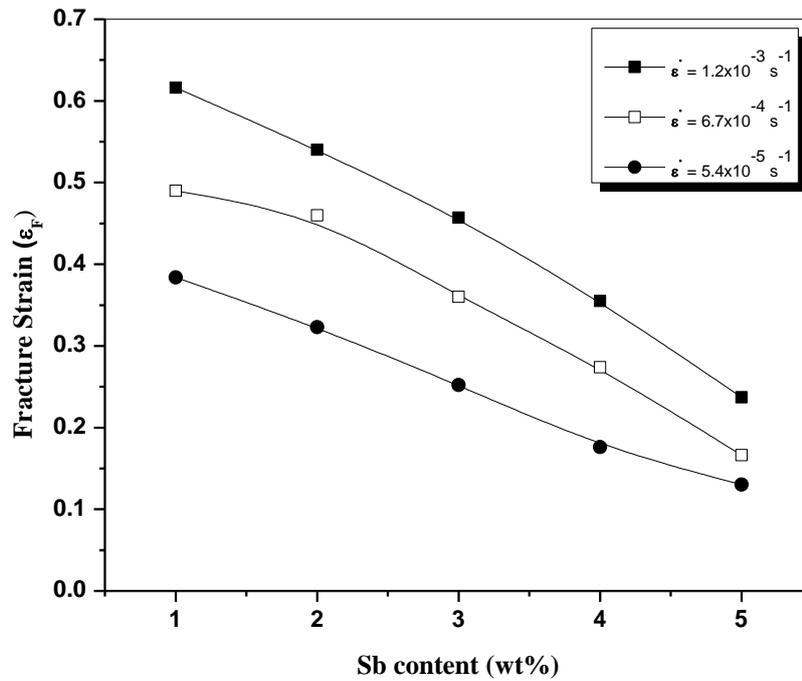


Figure 3. The dependence of fracture strain (ϵ_F) on the Sb-content at different strain rates (5.4×10^{-5} , 6.7×10^{-4} and $1.2 \times 10^{-3} \text{ s}^{-1}$)

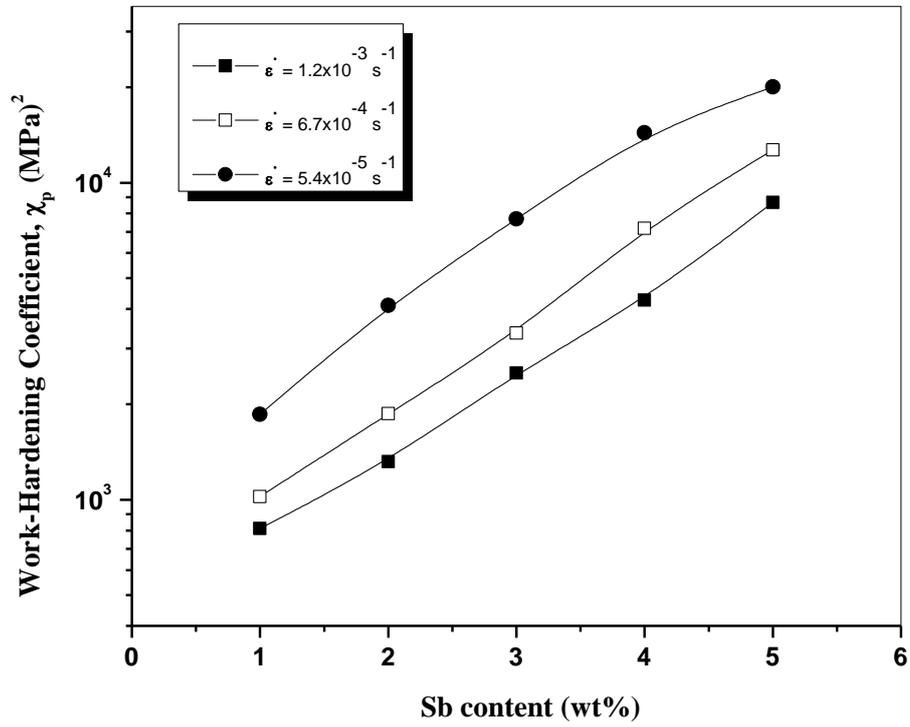


Figure 4. The dependence of work hardening coefficient χ_p on the Sb-content at different strain rates (5.4×10^{-5} , 6.7×10^{-4} and $1.2 \times 10^{-3} \text{ s}^{-1}$)

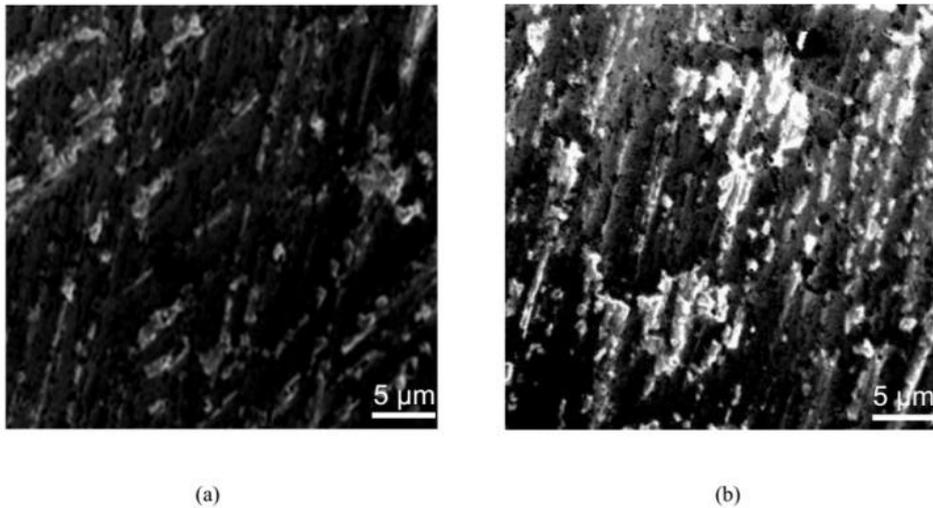


Figure 5. SEM micrographs at room temperature for: (a) un-strained Pb-1wt% Sb and (b) un-strained Pb-5wt% Sb alloy

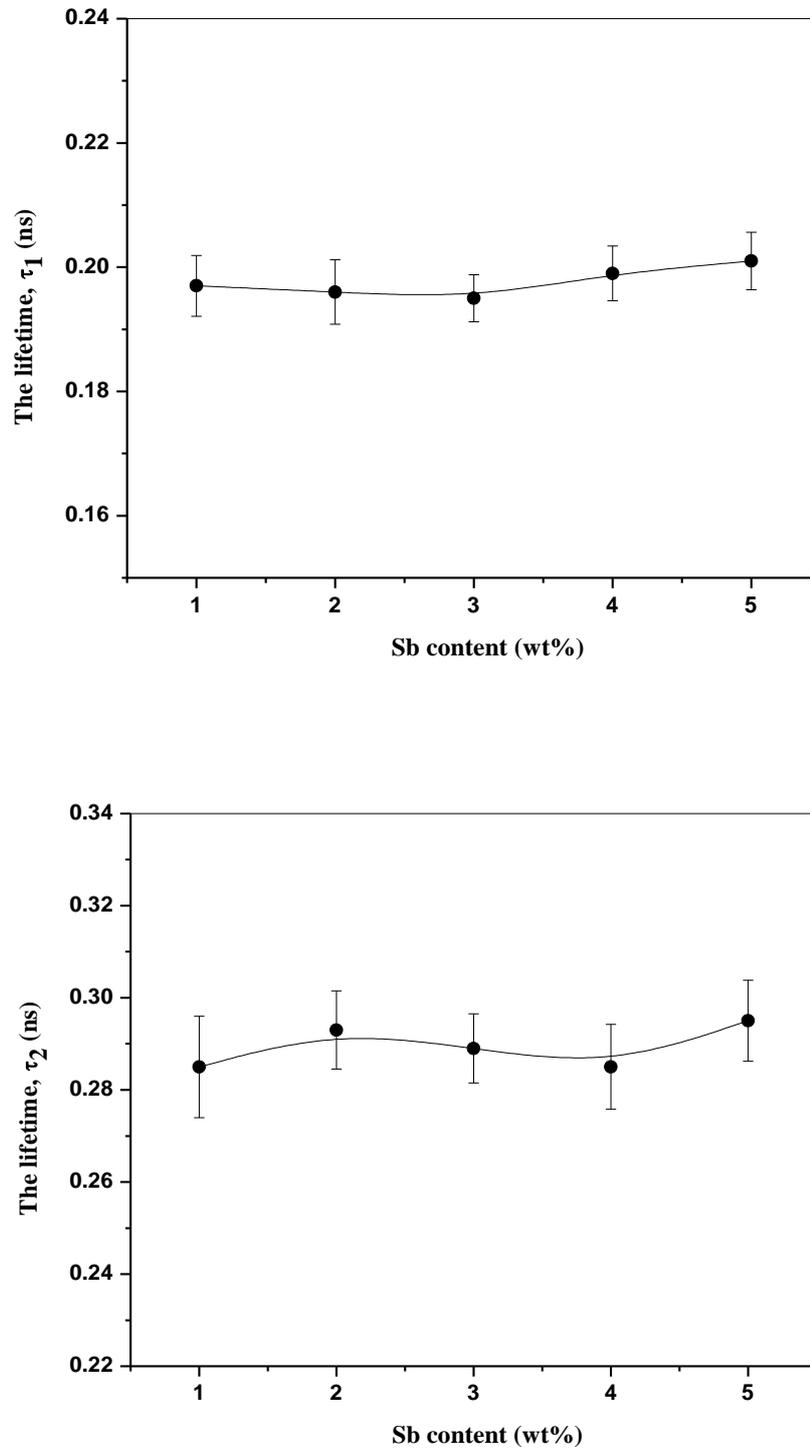


Figure 6. The change in the lifetime components τ_1 and τ_2 with increasing Sb-content

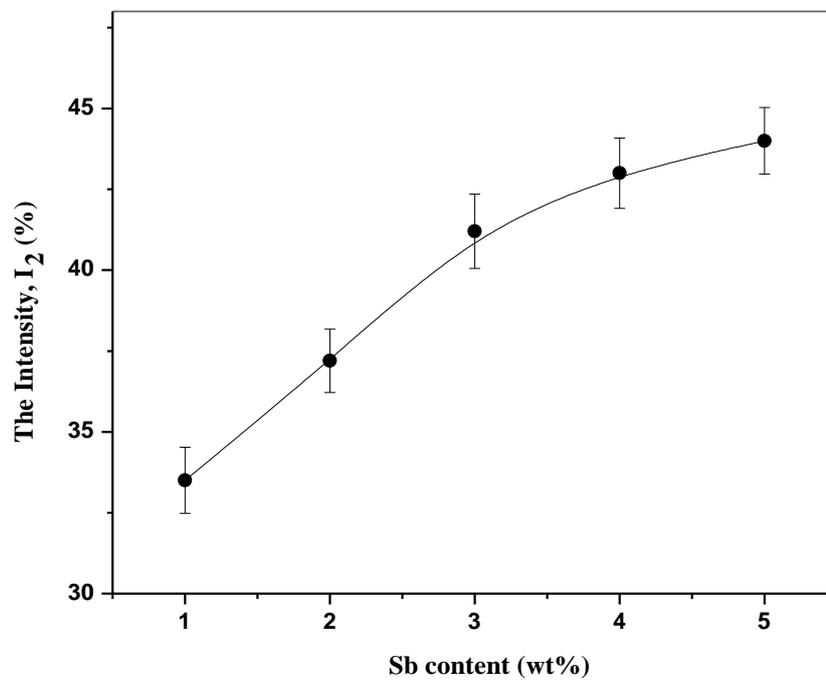
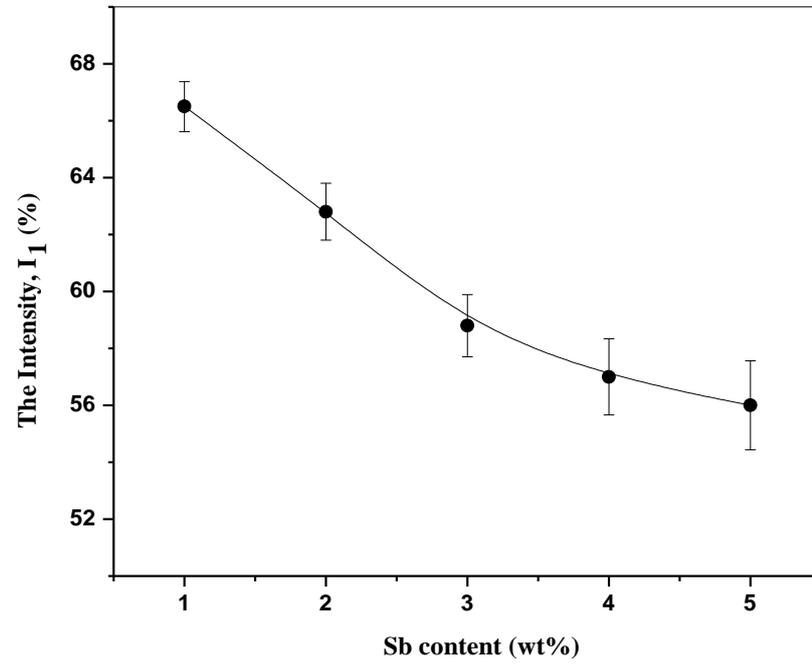


Figure 7. The change in the intensities I_1 and I_2 with increasing Sb-content

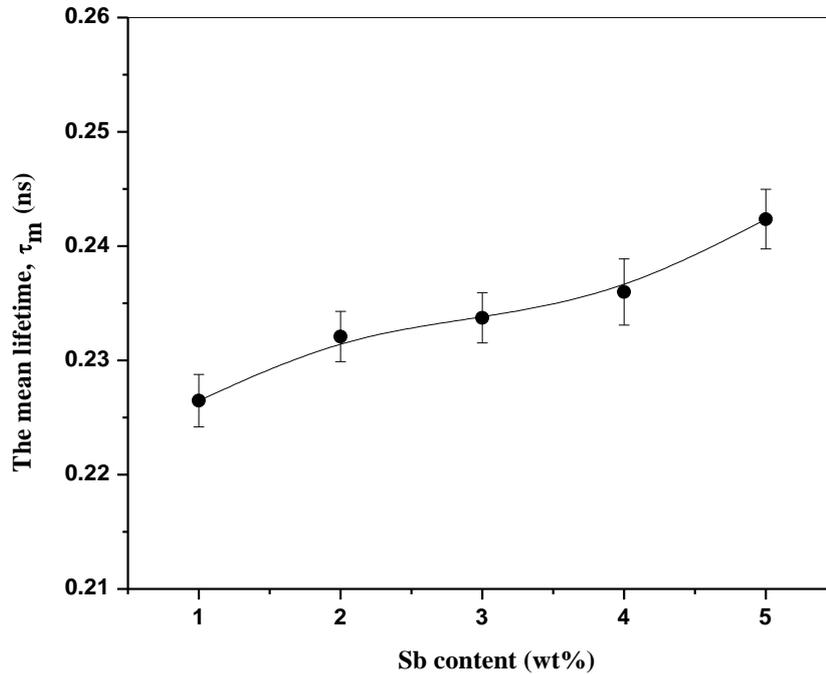


Figure 8. The dependence of mean lifetime (τ_m) on the Sb-content

To investigate the effect of ε^\bullet on σ_F and ε_F , there is a popular relation that correlates between σ_F and ε^\bullet which is Norton's power law;

$$\sigma_F = C (\varepsilon^\bullet)^m \quad (3)$$

where C is a constant and m is the strain rate sensitivity index. From this equation [23], it is clear that, σ_F increases as ε^\bullet does. Indeed, there is a reverse relation between σ_F and ε_F , i.e., increasing σ_F decreases ε_F . Indeed, increasing ε^\bullet increases the density of dislocations so the movement of dislocations and Sb-rich phase was hindered which results in an increase σ_F and a decrease in ε_F . As the value of ε^\bullet increases its effect on σ_F , χ_p and ε_F will be more evident.

The aforementioned arguments could help in accounting for the data presented in Figs. (2-4).

The analysis of positron annihilation lifetime data by LT 9.0 gives two lifetime components (τ_1 and τ_2) and two corresponding intensities (I_1 and I_2), see Figs (6, 7). τ_1 is the shorter lifetime, its value is 0.195 ns, and it's independent of Sb content. This value agrees with the positron lifetime in bulk Pb (0.198 ns) [13]. The positron annihilation in bulk Pb represents the main probability because of the high concentration of Pb in the present alloys (see Table (1)) this explains the higher values of I_1 (56-67%). The second lifetime component (τ_2) is the long lifetime, its value is about 0.288 ns, it is much higher than the positron lifetime in bulk Pb. It was suggested that τ_2 represents positron annihilation at the interfaces between Pb-rich phase and Sb-rich phase, see figure 5. It should be mentioned that, there is no chance to compare our findings in this part with those of others for

the reason mentioned in the introduction. Also, some investigators [24, 25] studied this phenomena, but in other solids. With increasing Sb-content, the intensity (I_1) decreases because the probability of positron annihilation (or the fraction of positrons annihilated) in the bulk Pb decreases and consequently such probability at the interfaces increases (I_2 increases). The increase in the mean lifetime τ_m as Sb-content increases (see figure 8) may be due to the higher probability of positron annihilation at the interfaces between Pb-rich phase and Sb-rich phase.

5. Conclusions

The effect of Sb-content and strain rate on the work hardening characteristics in Pb-1-5wt% Sb alloys were studied by stress-strain measurements and positron annihilation lifetime spectroscopy. It was found that, (i) increasing Sb-content at constant ε^\bullet , increases the fracture stress σ_F and work hardening coefficient χ_p while the fracture strain ε_F decreases (ii) for each alloy, with increasing ε^\bullet , σ_F and χ_p decreases while ε_F increases (iii) with increasing Sb-content, the lifetime component τ_1 is nearly constant and its value is 0.195 ns. Also τ_2 is invariable with value about 0.288 ns which may represent positron annihilation at the interfaces between Pb-rich phase and Sb-rich phase (iv) the intensity I_1 decreases with increasing Sb-content while I_2 and the mean lifetime (τ_m) increase.

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