

The Impact of Machining Parameters on Peak Power and Energy Consumption in CNC Endmilling

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Abstract Machining in a production environment commonly relies on trying maximizing material removal rates (MRR). This is done at the expense of increased peak power loads on the machine tool and machine spindle, and at the expense of potentially increasing energy consumption. To begin to develop an understanding of the relationship between peak power and energy consumption with machining parameters, spindle and total machine tool power are measured directly during a series of dry and wet endmilling tests on a 3-axis CNC milling machine. Cutting speeds, feedrates, and endmill immersions are varied and the resulting peak power measurements analyzed. Increasing any one of these parameters increases MRR and the peak power loads of the spindle and machine tool. However, the actual energy consumption varies widely for each parameter and in some cases such as when we increase feedrates, can actually decrease dramatically. The results of the direct measurements are presented and discussed as they relate to metal cutting.

Keywords Spindle Power, CNC Machining Power, Energy Management, Energy Consumption, Machining

1. Introduction

Recent reports have shown the manufacturing sector to account for 23% of the energy used in Canada[1], and as much as 30% of the energy used in the United States[2]. Increasing energy costs, environmental awareness, and continued pressure to reduce cycle times and costs have caused manufacturers to consider environmental practices and energy consumption as it relates to their facilities and specific processes. Power measurement is not new to metal cutting, motor power consumption has been used to assess and predict tool wear and fracture as an alternative to using force measurement. Mannan et al.[3] and Cuppini et al.[4] were two of the first groups of researchers to actively monitor machine tool power in turning and milling, respectively, concluding that power signals are highly effective at detecting tool breakage, but reasonably insensitivity to continual tool wear. Several studies have examined the drilling process. Choi et al.[5] used feed motor current, Kim and Ahn[6] focussed on signals from the machine tool control unit, and Li and Tso[7] measured the motor current signal externally to predict drill failure. A similar approach has also been taken by Patra et al.[8] to examine flank wear, and coupled with acoustic signal processing, has been used to detect tool wear and breakage[9].

One of the first studies to examine energy usage of computer numerical controlled (CNC) machines was done by Filippi et al.[10]. This study found that the largest loss of efficiency in machining was due to machine under-utilization. Following this early study, several researchers focussed efforts on developing models to predict energy consumption of various machine tools. From computer aided design and manufacturing (CAD/CAM) data, Avram[11] developed a program to predict energy usage requirements based on tool path information, tool geometry, and cutter parameters. Electrical and mechanical losses are difficult to determine and as such, difficult to integrate into this approach. As well, machine characterisation would be necessary to properly analyse each process.

Using Specific Energy Consumption (SEC) theory, Kara [12] developed an empirical model to predict energy consumption in machine tools that was dependent on MRR and workpiece material properties. The approach considered energy consumption in the cutting process exclusively. Use of empirical models is limited however without considering the cutting mechanics, tool behaviour, and the actual machine tool itself. The mechanics of the machining process can be broken down such that the cutting power can be estimated, but these formulations would be highly inaccurate as the cutting tool wears, process parameters change, material dynamic behaviours change, or there are changes in the machine tools used or machine tool performance due to maintenance. To have a better degree of accuracy, each machining process for a specific workpiece material would have to be considered and an empirical formulation used for each case which has not been done to date.

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Peripherals associated with time for setup, standby, positioning, and coolant, were ignored. Diaz *et al.*[13] furthered the work by predicting energy consumption for tool paths with varying MRR. While they reported an average accuracy of 97.4%, the approach again neglected energy consumption outside of the metal cutting process. Developing an energy prediction model Bi *et al.*[14] used their predictive model to reduce power consumption and produce an optimal set of machining process parameters, adding a surface roughness prediction model to this approach to obtain a minimum level of surface quality[15]. The approach and results are very machine tool specific.

The previously mentioned works focussed on predictive and in some cases idealized modelling of power consumption. In recent efforts to use active approaches for monitoring of power consumption, Weinert *et al.*[16] demonstrated that the power signal from the machine tool could be decomposed into constant and variable components. Using a standard test part Behrendt *et al.*[17] compared the energy consumption of various machine tools and noted a substantial difference between machine tools, concluding that a standardized practice for assessing and publishing machine tool energy consumption could be beneficial. Hu *et al.*[18] examined CNC turning, measuring input power only of a machine tool. Mori *et al.*[19] looked at deep-hole drilling, face and endmilling, and drilling operations. They found that by reducing processing times (maximizing MRR), a reduction of power in milling and drilling could be realized. From ball end milling experimentation, Oda concluded that to minimize energy consumption it is necessary to maximize the undeformed chip thickness[20].

While there is a recognized need for energy efficiency in manufacturing, a review of energy efficiency research in 2011 revealed a wide gap between what academic researchers have reported versus what industry can implement[21]. Modelling energy consumption mathematically, Mativenga and Rajemi[22] noted an apparent synergy between energy consumption and production cost. Similarly, He *et al.* concluded that energy consumption could be an effective input to multi-objective process planning procedures[23, 24]. For the current work, the spindle and the total machine tool power are directly measured for a series of endmilling experiments which has not been done to date in any of the literature. The impact of different cutting parameters as it relates to spindle and machine tool power consumption with respect to changes in MRR is presented and discussed.

2. Experimental

A defined set of endmilling experiments using a 3/8" diameter, 4-flute, carbide endmill, were conducted with the intent of directly measuring the power (in Watts) consumed by the machine tool and the machine spindle during machining. The impact of changing machining parameter such as cutting speeds, feedrates, and depths of cut, will be

analysed and presented with respect to MRR which is a primary motivator for adjusting machining parameters in the first place. The endmilling tests were carried out on an Okuma 4020 vertical milling machine and the same AISI 1045 steel workpiece was used in all of the machining trials.

In the first series of endmilling tests, the volume of material removed was kept constant and spindle speeds and feedrates varied from 75 to 100 m/min and 0.025 to 0.05mm/tooth respectively. With a constant volume, changes in speeds and feedrates translate into a change in MRR. In the next series of cutting tests, cutting time was kept constant and the axial and radial immersions of the endmill during cutting were varied from 0.25 to 2.0 mm and 25 to 100% (full slotting), respectively. By varying immersions and holding cutting speed and feedrate constant the volume of material to be machined would vary while holding process time constant, again leading to a change in MRR. These variables as they relate to the endmilling operation are shown in Figure 1. All cutting tests were first done dry and then repeated with coolant.

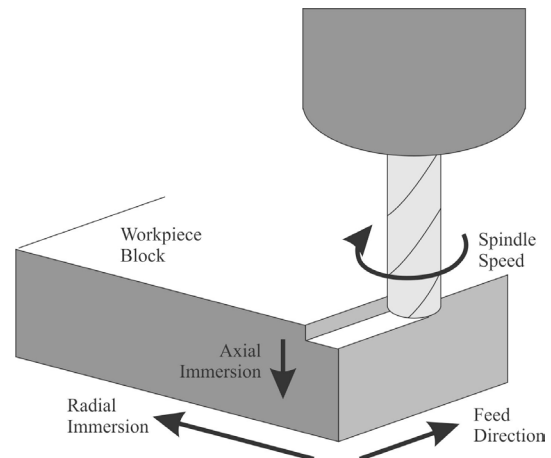


Figure 1. Overview of the endmilling process and process parameters

The spindle and total power signal was recorded and analysed for each series of cutting tests. The actual power monitoring was done using a three phase power transducer on the incoming power lines into the CNC milling centre and a three phase power transducer on the lines to the spindle motor. Signals were measured and recorded using a custom LabView program and interface. Both transducers were tested and calibrated to ensure their proper function.

3. Results and Discussion

From the series of constant volume and constant cutting time endmilling tests, the directly measured spindle and machine tool power was recorded. Results from each series of cutting tests are presented and discussed. While direct measurement of the power signals has been measured in Watts (W), as a result of the short machining cycle times, energy consumption has been calculated in kilojoules (kJ), rather than total power consumption which takes the form of a kilowatt-hour (kWh).

3.1. Increasing Speeds and Feedrates

Holding all other cutting parameters constant, an increase in spindle speed leads to a direct increase in MRR, and an increase in spindle and machine tool power draw as shown in Figure 2. Increasing the spindle speed from 2506 rpm (cutting speed of 75 m/min) up to 3341 rpm (cutting speed of 100 m/min), there is a substantial increase in peak power levels during cutting and non-cutting, and power consumption during cutting and non-cutting.

The non-cutting time in any process will typically be minimized, but it is worth noting that during non-cutting the spindle draws 400 W at the lower speed and 500 W at the higher speed as shown in the two lower power signals in Figure 2. This 100 W difference during non-cutting is also observed for the machine tool power or the two top most signals in Figure 2. The energy consumed by the spindle during these non-cutting time periods is 1.0 kJ and 1.25 kJ at the two prescribed spindle speeds. The peak machine power levels during non-cutting were 1150 W and 1250 W which equates to an energy draw of 2.875 kJ and 3.125 kJ for the two spindle speeds.

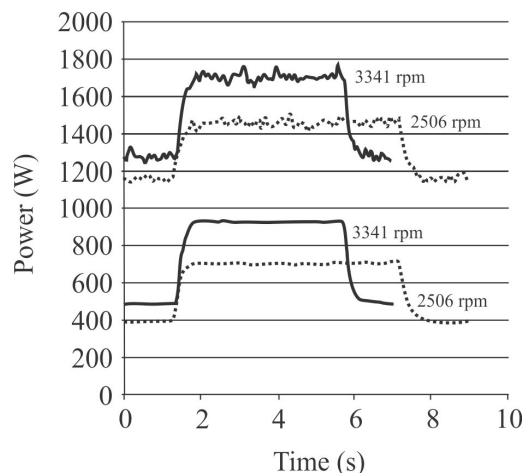


Figure 2. Measured machine power (top most curves) and spindle power (lower two curves) for different spindle speeds. Full slotting operation, axial depth, $a=1$ mm, and feedrate, $f=0.05$ mm/tooth

During actual cutting, the spindle peak power increased from 700 W (300 W increase from non-cutting) up to 910 W (410 W increase from non-cutting), and 1475 W up to 1700 W for the total machine tool. For these particular cutting tests, the measured power associated with the actual cutting process was less than that required to simply rotate the spindle at the prescribed speeds which is due to the light cuts that were used in the experiments, but any analysis to have practical applicability requires that the peak power and energy consumption associated with the free spinning spindle be included. As a result, during cutting the actual energy consumption of the spindle remained constant at 4.2 kJ irrespective of spindle speed, and the total energy consumed by the machine tool actually decreased from 8.7 kJ down to 7.8 kJ as the speed increased. These energy consumption results are summarised in Table 1.

Table 1. Spindle and machine tool energy consumption for different spindle speeds

Spindle Speed (rpm)	Spindle Energy (kJ)		Machine Energy (kJ)	
	In-Cut	Total	In-Cut	Total
2506	4.2	5.2	8.7	11.68
3341	4.2	5.45	7.8	10.98

The energy consumption of the spindle for the cutting process exclusively is 1.8 kJ, which is the equivalent of 15% and 16% of the total energy consumed at the lower and higher speeds, respectively. It should be a goal to maximize the percentage of the total energy consumption associated with actual cutting, which is the rationale for minimizing pre- and post-cutting portions of any machining cycle. For these particular tests, the increase in cutting speed leads to a reduction in cycle time and subsequent increase in MRR of approximately 33%. Using spindle speed alone to increase MRR will have little effect on the overall energy consumption of the spindle. However, there is an overall energy consumption decrease for the total machine tool which is a direct result of the reduction in cycle time.

The minimal impact on the energy consumption of the spindle and slight decrease in machine tool energy consumption can be related to the cutting process. With all other cutting parameters constant, the increase in cutting speed does increase the resulting cutting forces acting on the endmill and thus, there is an increase in the peak power required by the machine spindle. The increased peak power draw of the spindle and machine tool is offset by the decrease in process time which leads to only a small decrease in the energy consumption as a result of a change in cutting speed.

Increasing MRR by increasing feedrates exclusively decreases cycle times while increasing chip load on the cutting tool. The effect on spindle and overall machine tool power measurements is shown in Figure 3. When the feedrate doubles, cycle time is cut in half, and the MRR increases by 100%. Whether considering only the total power draw of the spindle and machine tool or just the cutting portion, the total power draw decreases substantially in all cases as summarised in Table 2.

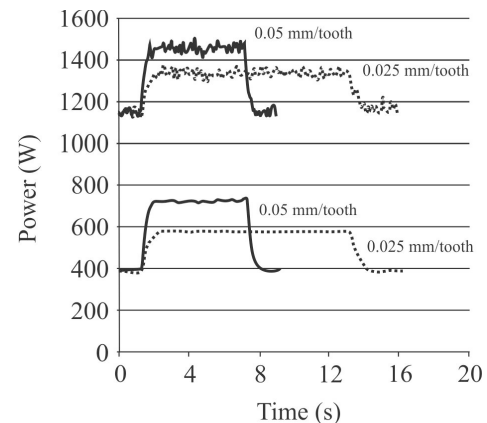


Figure 3. Measured total machine power (top most curves) and spindle power (lower two curves) for different machine feedrates. Full slotting operation, axial depth, $a=1$ mm, and cutting speed is 2506 rpm

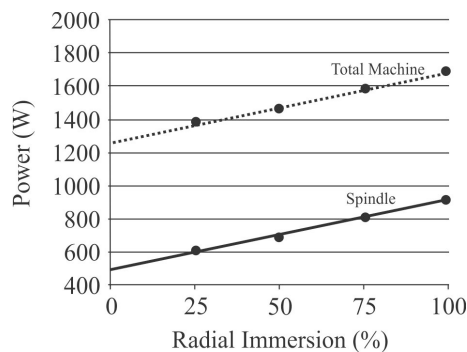
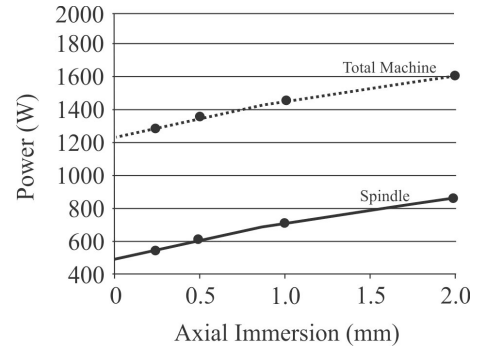
Table 2. Spindle and machine tool energy consumption for different feedrates

Feedrate (mm/tooth)	Spindle Energy (kJ)		Machine Energy (kJ)	
	In-Cut	Total	In-Cut	Total
0.025	7.0	8.6	16.0	21.0
0.05	4.2	5.45	8.7	12.2

A 100% increase in MRR as a result of doubling the feedrate leads to an overall energy consumption decrease of 37% for the spindle and a 42% decrease for the machine tool. Comparing the non-cutting to actual cutting process, the peak spindle power increased from 400 W up to 580 W (180 W increase) at a feedrate of 0.025 mm/tooth. When the feedrate doubled, the peak spindle power increased to 700 W (an increase of 300 W). A doubling of feedrate will not simply lead to a doubling of spindle power during cutting. This again is explained by considering the cutting process and specifically the workpiece material properties during the cutting process. Increasing the chip load increases cutting forces which are a function of the cutting parameters and workpiece material properties. The relationship between workpiece material properties (in this case AISI 1045 steel) and the actual cutting process is not a simple linear relationship and is much more complicated. Depending on the materials dynamic behaviour during the cutting process, it is possible that as feedrates are increased, not only will there be a reduction in cycle time, but the subsequent increases in peak power could decrease and the total energy consumption of the process could be reduced further.

3.2. Radial and Axial Immersion

For the constant cutting cycle time tests, radial and axial immersions were varied to increase MRR during endmilling. Increasing the radial and axial immersion of the endmill leads to an increase in the peak spindle and machine tool power is shown in Figure 4 and Figure 5 as a result of the increased load on the cutting tool. Increasing the radial immersion (and subsequently the MRR) by 300% leads to a spindle power consumption increase of approximately 54%. Increasing the axial immersion by 700% leads to an increase of approximately 50% in spindle power consumption. A substantial increase in MRR can be realized with a relatively small increase in power consumption.

**Figure 4.** Total machine and spindle peak power measurements for different radial immersions. Spindle speed is 2506 rpm and the feedrate is 0.05mm/tooth**Figure 5.** Total and spindle power measurements for different axial immersions. Spindle speed is 2506 rpm and the feedrate is 0.05mm/tooth

From the radial immersion results, there would appear to be a linear relationship between power consumption and immersion for this specific endmill, machine tool, and workpiece material. These results can be related back to the machining process. Increases in radial immersion up to 50% will increase the chip load along a single cutting edge. Beyond 50% immersion, the chip load no longer increases, but a second cutting edge engages with the workpiece which adds to the forces being seen by the cutting tool. This translates into increased spindle and machine tool power consumption. When increasing the axial immersion of the endmill during cutting it appears that with each increase in axial immersion, the subsequent increase in power consumption becomes less. The axial immersions in these trials were relatively small. Therefore, for a full slotting operation with a 4-flute endmill only two cutting edges were engaged with the workpiece at any point in time. If the axial immersion increases enough, the number of contact points between cutting edges and the workpiece could increase, leading to a rise and subsequent increase in power requirements for the spindle and machine tool. Each time there is a new contact point between a cutting edge and the workpiece material, the power consumption as a result of axial immersion will increase.

3.3. Impact of Using Coolant

The auxiliary systems associated with coolant have been ignored in previous work, but coolant can be beneficial to the cutting process, improving cutting performance and tool life. A comparison of the results from Figure 2 with Figure 6, and Figure 3 with Figure 7 highlights that there is no change in the peak power requirements of the spindle during the non-cutting stages of the experiments irrespective of the presence of coolant which is expected. However, when comparing the cutting portion of the measured peak power, the use of coolant leads to a decrease of 50 W in the peak power required by the spindle. This slight decrease is a result of the coolant acting as a lubricant during the cutting process and subsequently reducing cutting forces.

The reduction in peak spindle power as a result of the use of coolant may be more relevant for finishing operations such as those used in the current study where peak spindle power increases may only be 200-300 W, as compared to

roughing operations which could exceed 1 kW. The reduction in peak spindle power however is negligible compared to the subsequent impact on the peak power of the machine tool overall as shown in Figure 6 and 7. With the addition of coolant to the cutting process, there is a peak power increase of an additional 500 W.

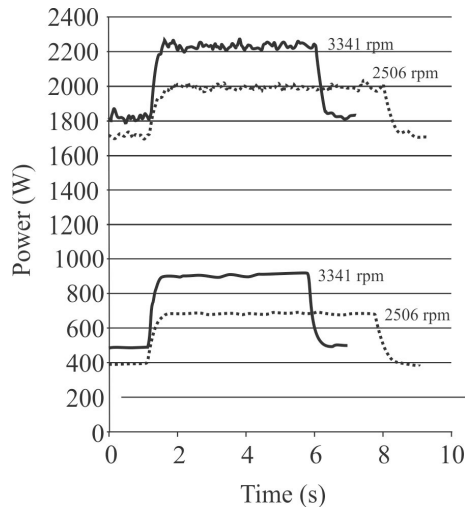


Figure 6. Measured machine power (top most curves) and spindle power (lower two curves) for different spindle speeds. Full slotting operation, axial depth, $a=1$ mm, and feedrate, $f=0.05$ mm/tooth with the use of coolant

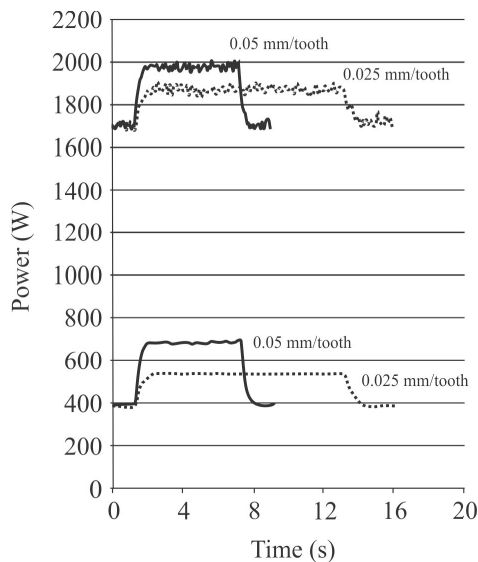


Figure 7. Measured total machine power (top most curves) and spindle power (lower two curves) for different machine feedrates. Full slotting operation, axial depth, $a=1$ mm, and cutting speed is 2506 rpm with the use of coolant

The 500 W power consumption increase of the machine tool is substantial for these machining tests. Had this been a roughing process, this power increase would have still occurred, but its impact might not be as substantial if the use of coolant can be used to reduce potential cycle times or increase MRR.

Based on the results of the direct measurements it is clear that attempts to increase MRR may actually have a net beneficial effect on energy consumption even though peak power levels will increase. The use of any auxiliary

equipment such as the equipment used for coolant should also be included in any analysis. The development and implementation of a peak power or energy management strategy will require proper characterisation of individual machine tools, cutting processes, and machining of different workpiece materials.

The results presented are only for one specific machine under specific cutting conditions. Changes to tooling, setup, or workpiece material would yield different results. While individual machining parameters were examined in the experiments, it is the proper combination of these parameters that manufacturers will use to maximize MRR. The combination of machining parameters has not been considered to date, but conducting more experiments with direct power measurement will allow for the creation peak power and energy consumption contours for different processes and components. These contours could be used to map an energy efficient manufacturing strategy.

Proper endmilling cutting parameter selection can lead to a dramatic increase in MRR without a dramatic increase in energy consumption the machine spindle or the machine tool overall. The initial analysis of spindle and machine tool energy consumption highlights the need to develop a proper strategy based on peak power, total energy consumption, and specifics regarding the machining process as part of an overall framework to examining and making effective decisions regarding machining process changes as they relate to energy management.

There is a need to extend the current work to cover to more closely examine the peak power signal of the machine tool during the machining process. This would include isolating and examining other primary elements of the machine tool such as feed drives, controllers, pumps, and compressors. Thus, a more complete power and energy consumption map can be created for machined components. An alternative is to quantify the power usage for specific tooling, machines, and cutting conditions to create a comprehensive energy management schema, beyond a basic empirical approach so as to ensure more reliable results for predictive purposes.

4. Conclusions

From direct power measurement of the spindle and machine tool during endmilling tests, the impact of different machining parameters on peak power and energy consumption of the total machine tool and machine spindle for a 3-axis CNC milling machine was examined. Increasing spindle speeds (cutting speed), feedrates, and tooling immersions leads to an increase in MRR. This leads to an increase in peak power of both the spindle and the machine tool, but the impact on energy consumption is not universal. Increased spindle speeds and feedrates increases MRR and can actually lead to an overall energy consumption decrease. By increasing immersions, substantial increases in MRR can be realized with only a small relative increase in energy consumption. The current results are machine tool,

workpiece material, and cutter specific, but the process and methodology used can be replicated on other machine tools. An analysis of the impact of individual cutting parameters does not allow for a comprehensive conclusion to be drawn regarding optimal cutting conditions to minimize peak power and energy consumption; however it does represent a practical starting point for power analysis in metal cutting. For manufacturers with standardized product lines, this approach could be implemented quickly, and could be useful in identifying potential energy and cost savings measures.

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REFERENCES

- [1] The Canadian Manufacturing Industry: Investments and Use of Energy-Related Processes or Technologies. Technical report, Statistics Canada, 2009.
- [2] Manufacturing Energy Consumption Survey (MECS): Total Consumption of Electricity by Manufacturing Industry and Region. Technical report, US Energy Information Administration, 2013.
- [3] M.A. Mannan, S. Broms, and B. Lindstrom, "Monitoring and Adaptive Control of Cutting Process by Means of Motor Power and Current Measurements", *CIRP Annals - Manufacturing technology*, vol. 38(1), p. 347-350, 1989.
- [4] D. Cuppini, G. D'Errico, and G. Rutelli, "Tool Wear Monitoring Based on Cutting Power Measurement", *Wear*, vol. 139(2), p. 303-311, 1990.
- [5] Y.J. Choi, M.S. Park, and C.N. Chu, "Prediction of Drill Failure using Features Extraction in Time Frequency Domain of Feed Motor Current", *International Journal of Machine Tools and Manufacture*, vol. 48(1), p. 29-39, 2008.
- [6] H-Y. Kim and J-H. Ahn, "Chip Disposal State Monitoring in Drilling Using Neural network based Spindle Motor Power Sensing", *International Journal of Machine Tools and Manufacture*, vol. 42(10), p. 1113-1119, 2002.
- [7] X. Li and S.K. Tso, "Drill Wear Monitoring Based on Current Signals", *Wear*, vol. 231(2), p. 172-178, 1999.
- [8] K. Patra, S.K. Pal, and K. Bhattacharyya, "Artificial Neural Network Based Prediction of Drill Flank Wear from Motor Current Signals", *Applied Soft Computing*, vol. 7(3), p. 929-935, 2007.
- [9] D.R. Salgado and F.J. Alonso, "An Approach Based on Current and Sound Signals for In-Process Tool Wear Monitoring", *International Journal of Machine Tools and Manufacturing*, vol. 47(14), p. 2140-2152, 2007.
- [10] A.D. Filippi, R. Ippolito, and G.F. Micheletti, "NC Machine Tools as Electric Energy Users", *CIRP Annals - Manufacturing Technology*, vol. 30(1), p. 323-326, 1981.
- [11] I.O. Avram and P. Xirouchakis, "Evaluating the Use of Phase Energy Requirements of a Machine Tool System", *Journal of Cleaner Production*, vol. 19(67), p. 699-711, 2011.
- [12] S. Kara and W. Li, "Unit Process Energy Consumption Models for Material Removal Processes", *CIRP Annals - Manufacturing Technology*, vol. 60(1), p. 37-40, 2011.
- [13] N. Diaz, K. Ninomiya, J. Noble, and D. Dornfeld, "Environmental Impact Characterization of Milling and Implications for Potential Energy Savings in Industry", 5th CIRP Conference on High Performance Cutting, p. 518-523, 2012.
- [14] Z.M. Bi and L. Wang, "Optimization of the machining Process from the Perspective of Energy Consumption: A Case Study", *Journal of Manufacturing Systems*, vol. 31(4), p. 420-428, 2012.
- [15] Y. Guo, J. Loenders, J. Duflou, and B. Lauwers, "Optimization of Energy Consumption and Surface Quality in Finish Turning", 5th CIRP Conference on High Performance Cutting, p. 512-517, 2012.
- [16] N. Weinert, S. Chiotellis, and G. Seliger, "Methodology for Planning and Operating Energy-Efficient Production Systems", *CIRP Annals - Manufacturing Technology*, vol. 60(1), p. 41-44, 2011.
- [17] T. Behrendt, A. Zein, and S. Min, "Development of and Energy Consumption Monitoring Procedure for Machine Tools", *CIRP Annals - Manufacturing Technology*, vol. 61(1), p. 43-46, 2012.
- [18] S. Hu, F. Liu, Y. He, and T. Ju, "An On-line Approach for Energy Efficiency Monitoring of Machine Tools", *Journal of Cleaner Production*, vol. 27, p. 133-140, 2012.
- [19] M. Mori, M. Fujishima, Y. Inanmasu, and Y. Oda, "A Study on Energy Efficiency Improvement for Machine Tools", *CIRP Annals - Manufacturing Technology*, vol. 61(1), p. 145-148, 2011.
- [20] Y. Oda, M. Mori, K. Ogawa, S. Nishida, M. Fujishima, and T. Kawamura, "Study of optimal Cutting Condition for Energy Efficiency Improvement in Ball End Milling with Tool-Workpiece Inclination", *CIRP Annals - Manufacturing Technology*, vol. 61(1), p. 119-122, 2012.
- [21] K. Bunse, M. Vodicka, P. Schnsleben, M. Brhlhart, and F.O. Ernst, "Integrating Energy Efficiency Performance in Production Management Gap Analysis Between Industrial Needs and Scientific Literature", *Journal of Cleaner Production*, vol. 19(67), p. 667-679, 2011.
- [22] P.T. Mativenga and M.F. Rajemi, "Calculation of Optimum Cutting Parameters Based on Minimum Energy Footprint", *CIRP Annals - Manufacturing Technology*, vol. 60(1), p. 149-152, 2011.
- [23] A. Bruzzone, D. Anghinolfi, M. Paolucci, and F. Tonelli, "Energy-Aware Scheduling for Improving Manufacturing Process Sustainability: A Mathematical Model for Flexible Flow Shops", *CIRP Annals - Manufacturing Technology*, vol. 61(1), p. 459-462, 2012.
- [24] Y. He, B. Liu, X. Zhang, H. Gao, and X. Liu, "A Modeling Method of Task-Oriented Energy Consumption for Machining Manufacturing Systems", *Journal of Cleaner Production*, vol. 23(1), p. 67-174, 2012.