

# Study of Wear Behaviour of Recycled Metal Powder Filled Epoxy Composites Using Factorial Analysis

M. Sudheer

Department of Mechanical Engineering, St Joseph Engineering College, Mangaluru, Karnataka, India

**Abstract** Epoxy composites were prepared by using reprocessed metal dust powder as filler by varying the filler content. The basic mechanical properties such as density and hardness and dry sliding wear performance were evaluated as per ASTM standards. Wear tests were conducted on samples using pin-on-disc machine for different parameters as per full factorial design approach. It was found that filler has contributed to the density and hardness of the epoxy polymer. Factorial analysis indicated that both friction and wear were predominantly influenced by the metal powder content. The study demonstrated that waste metal powders have good potential to be used as filler for thermosets like epoxy.

**Keywords** Metal filler, Epoxy, Friction, Wear

## 1. Introduction

The friction and wear study of polymer composites have been of practical interest for over a half century. Polymers are usually compounded with various fillers on micro and nano-scale to improve its performance under different wear conditions [1]. Recently low cost fillers from industrial waste such as fly ash, red mud, flue dust, paper waste, recycled metals and alloy particles etc. are used as fillers for polymers and resulted in the improvement of properties of base polymers. Such an attempt also reduces cost of the final product as these fillers replace the costly polymer portion in the composites [2].

Several literatures are available on use of metal particles as fillers for polymers which has provided special functionalities such as optical [3], electrical [4-6], magnetic [7], thermal [6, 8, 9], mechanical [5, 6, 10-12] and tribological properties [8, 9, 12-16]. Metal polymer composites are also used in sensors and actuators in biomedical applications [17, 18]. The issues specific to the formation of metal polymer composites and their interfaces which are critical to its application are also addressed in the literatures [19].

The current study is concerned with the mathematical approach to the wear study of recycled cast iron powder filled epoxy composites.

## 2. Experimental Details

\* Corresponding author:

msudheerm2002@yahoo.co.in (M. Sudheer)

Published online at <http://journal.sapub.org/materials>

Copyright © 2016 Scientific & Academic Publishing. All Rights Reserved

### 2.1. Materials

Room temperature curing epoxy resin (LY556) belonging to the diglycidyl ether of bisphenol A (DGEBA) family along with the amino based hardener (HY951) supplied by Huntsman Advanced Materials India Pvt., Ltd., Bengaluru, India was used as the matrix material. Cast iron powders collected from the machine shop are first segregated in sieve shaker to obtain fine sized powders ( $\leq 50 \mu\text{m}$ ) and are then heated at  $400^\circ\text{C}$  in muffle furnace for two hours. This heating is done to ensure the removal of foreign particles from the powders.

### 2.2. Sample Preparation

Composites are prepared with the varying percentage of metal powders (0, 10 and 20 wt%) using casting procedure. The large difference in density of cast iron powders and epoxy posed a great challenge in casting process. Extreme care is taken to avoid the settling effect of metal particles in epoxy by continuously keeping it under stirring condition. The procedural steps in the casting process are presented elsewhere [20]. Test samples are coded as C0, C10 and C20 where numerals indicate the percentage of metal filler in composite.

### 2.3. Characterization of Test Samples

All tests were performed at room temperature and as per ASTM standards. Density was measured according to ASTM D792 using Archimedes Principle. Hardness of developed test samples was measured using Rockwell's Hardness Tester on M-Scale as per ASTM D785. Wear tests were conducted on pin-on-disc wear apparatus and wear test results are presented in terms of specific wear rate and coefficient of friction as per ASTM G99-05 (2016). Three

parameters, namely, sliding velocity (A), normal load (B), and filler content (C) each at three levels, are considered in the full factorial design. Control parameters and their levels are indicated in Table 1. A statistical analysis of variance (ANOVA) was performed to identify the control parameters and their interactions that are statistically significant. The statistical analysis was performed using MINITAB 14 statistical software package.

**Table 1.** Control factors and their levels used in the experiment

Control factor	Level		
	I	II	III
A: Sliding velocity (m/s)	1	2	3
B: Normal load (N)	15	30	45
C: Filler content ( wt%)	0	10	20

### 3. Results and Discussion

#### 3.1. Density and Hardness

The density and the hardness of the hybrid composites are listed in Table 2. It can be observed that the inclusion of the metal filler has contributed to improve the density and the hardness of the epoxy polymer. This is an expected behaviour that metal fillers being denser and harder will obviously improve the density and hardness of the base polymer.

**Table 2.** Density and Hardness of test samples

Material	Density (g/cc)	Hardness
C0	1.11	83
C10	1.24	87
C20	1.31	93

#### 3.2. Effect of Control Parameters on Friction and Wear

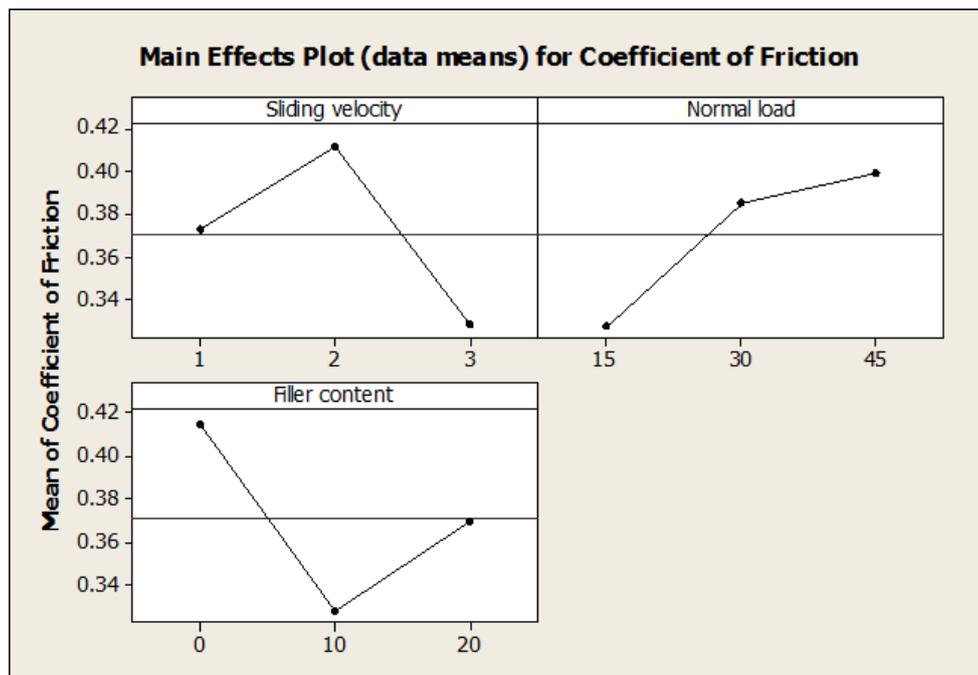
The design matrix for three control factors each at three levels along with the results of the wear tests are presented in Table 3. The influence of each control factor on the wear behaviour can be analysed with the main effects plot and interaction plot. The best combination of the control factors to optimize the performance output can be easily evaluated from this plot. In the main effects plot, if the line for a particular parameter is nearly horizontal, the parameter has a little effect. A parameter for which the line has the highest inclination has a greater effect [21]. The main effects plot for the parameters affecting the friction is presented in Figure 1. It is clear from the plot that all the three control parameters have shown considerable influence on friction coefficient. The increase in the sliding velocity has shown increasing and decreasing trend in the friction coefficient, whereas metal filler content has shown decreasing and increasing trend. However, normal load is found to continuously increase the friction coefficient. The effect of control parameters on the friction is a complex phenomenon in polymer tribology and is governed by many factors acting simultaneously. The effect of sliding velocity on friction coefficient can be explained as follows. With the increase of the speed from

1 m/s to 2 m/s, material loss from the composite surface increases and this result in the increase of the abrasive force due to the presence of hard cast iron particles at the sliding interface. This contributes to increase the friction coefficient values. With the further increase of the velocity up to 3m/s, the plastic deformation of the epoxy matrix dominates and forms a thin transfer layer between the sliding materials. The metal fillers aid in the retention of the friction film for a longer time. This results in the easy shear during the sliding and reduces the friction. It is seen that increase in normal load has increased the friction coefficient. This may be due to more loads required to cause the shearing with the increase in normal load. It can also be noted from Figure 1 that metal fillers have reduced the friction coefficient values. The presence of metal fillers may reduce the real contact area during sliding and more such fillers may cause less area in contact between the tribo-couples and result in low friction values. From the main effects plot is clear that parameters  $A_3B_1C_2$  resulted in minimum friction coefficient. The two-way interaction plot for friction coefficient is presented in Figure 2. It is well understood that interactions do not occur when the lines on the interaction plots are parallel and strong interactions occur when the lines cross [21]. This plot shows that the interaction effect of sliding velocity and filler content is the highest followed by sliding velocity  $\times$  normal load. Normal load and filler content has shown less interaction effects. The physical interpretation of these interactions is still a mystery.

The main effects plot for wear rate is presented in Figure 3. The main effects plot shows that filler content is the most significant parameter, while sliding velocity and normal load have relatively less significant influence. It is well known that tribological behaviour of polymers and polymer composites can be associated with their viscoelastic and temperature related properties. Sliding contact of two materials results in heat generation at asperities and hence increases the interface temperature, which influences the viscoelastic property in the response of material stress, adhesion, and transferring behaviours [22]. The increase in the sliding velocity increases the temperature at the friction surface and this could seriously deteriorate the mechanical properties of the composites and result in serious material loss. Thus, the wear rate increases when the sliding velocity is increased from 2m/s to 3m/s and it decreases when the velocity is increased from 1m/s to 2m/s. However, the increase in the normal load could result in early formation of transfer films, and further increase of the load could pack together the transfer films. These compressed and cohesive tribo-films are conducive to the reduction of the wear rate. Thus, wear rate showed a declining trend for the range of loads (15–45N) considered in the present study. It is clear from the main effects plot that metal fillers improved the wear resistance property of the polymer. Referring to Figure 3 the parameters  $A_2B_3C_2$  resulted in minimum wear rate. The interaction plot for specific wear rate is illustrated in Figure 4. An examination of Figure 4 yields a small interaction between the test parameters.

**Table 3.** Matrix for 3 × 3 full factorial design and corresponding test output

Experiment No.	Sliding velocity (m/s)	Normal load (N)	Filler content (%)	Friction Coefficient (FC)	Specific wear rate $\times 10^{-8}$ (mm <sup>3</sup> /Nm)
1	3	15	20	0.333	5.74567
2	1	15	10	0.300	2.50291
3	3	45	10	0.360	0.59593
4	3	30	10	0.156	0.35755
5	3	45	20	0.368	3.77412
6	2	15	0	0.427	9.20921
7	2	15	10	0.440	0.89389
8	3	15	10	0.126	0.17877
9	2	45	20	0.440	0.67596
10	1	15	20	0.220	4.05577
11	3	45	0	0.476	6.33967
12	3	15	0	0.360	9.60961
13	2	45	0	0.396	5.60561
14	2	45	10	0.335	1.01308
15	2	30	20	0.496	0.50697
16	1	45	20	0.446	4.84439
17	3	30	20	0.333	4.56274
18	2	30	10	0.413	0.71511
19	2	30	0	0.400	6.80681
20	1	45	0	0.373	3.33667
21	1	15	0	0.393	5.00501
22	1	30	20	0.340	5.49220
23	1	45	10	0.400	2.32413
24	1	30	10	0.423	2.32410
25	3	30	0	0.443	8.00801
26	1	30	0	0.463	4.20420
27	2	15	20	0.353	0.16899



**Figure 1.** Main effect plot for friction coefficient of test samples

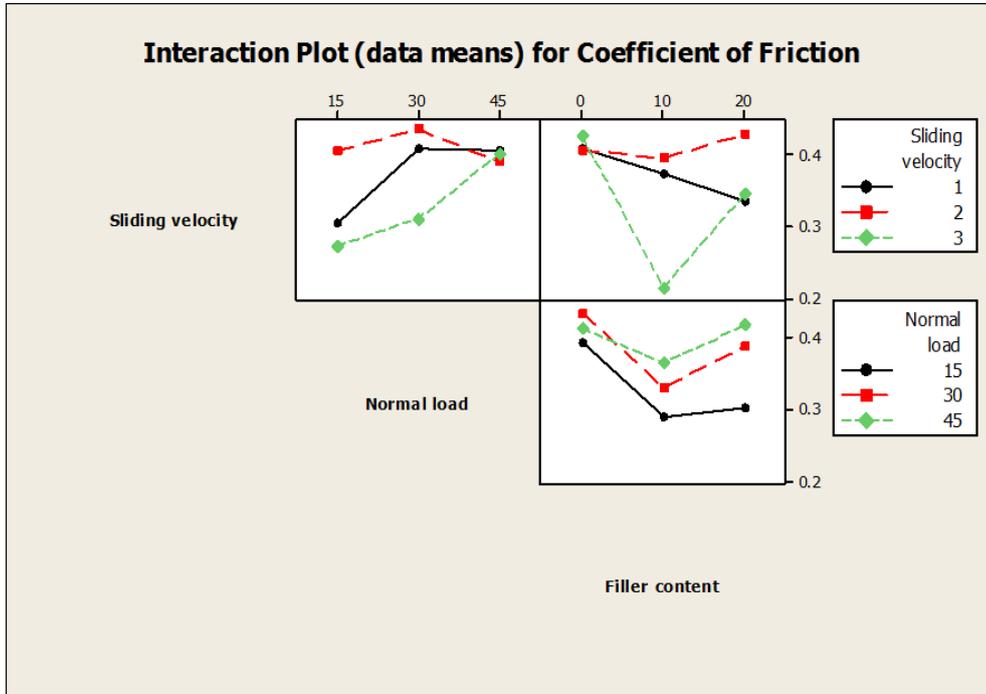


Figure 2. Interaction plot for friction coefficient of test samples

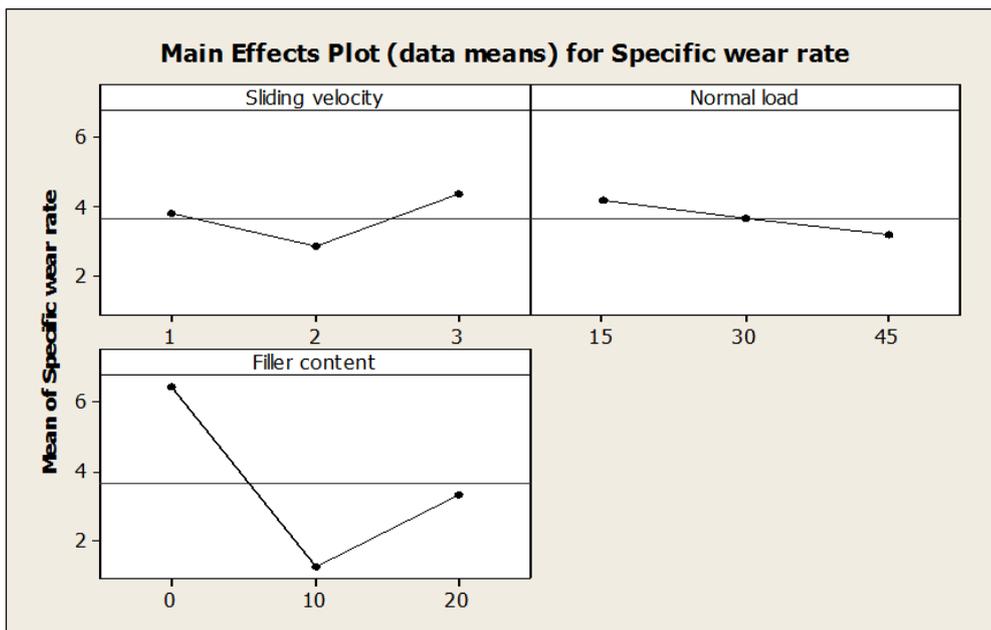


Figure 3. Main effect plot for wear rate of test samples

Table 4. ANOVA table for friction coefficient

Source	DOF	Seq SS	Adj SS	Adj MS	F-test	P-value	P (%)
Sliding velocity (A)	2	0.030904	0.030904	0.015452	3.29	0.090	15.03
Normal load (B)	2	0.025686	0.025686	0.012843	2.74	0.124	12.49
Filler content (C)	2	0.033639	0.033639	0.016820	3.59	0.07	16.36
A x B	4	0.024981	0.024981	0.006245	1.33	0.338	12.15
A x C	4	0.045238	0.045238	0.011309	2.41	0.135	21.99
B x C	4	0.007675	0.007675	0.001919	0.41	0.798	3.73
Error	8	0.037533	0.037533	0.004692			18.25
Total	26	0.205655					100

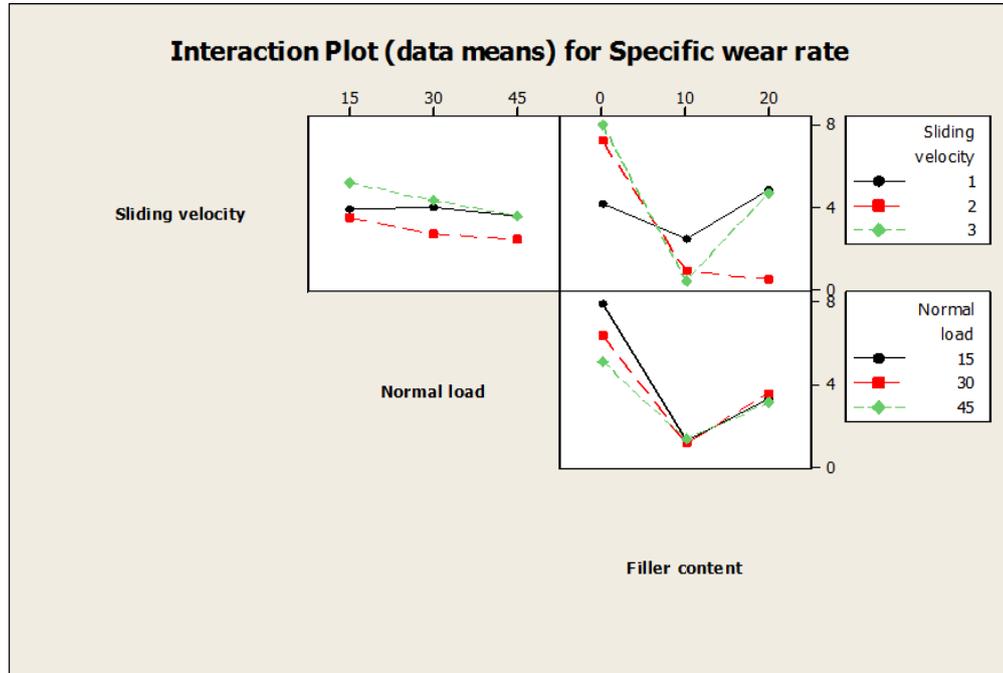


Figure 4. Interaction plot for wear rate of test samples

Table 5. ANOVA table for specific wear rate

Source	DOF	Seq SS	Adj SS	Adj MS	F-test	P-value	P (%)
Sliding velocity (A)	2	10.455	10.455	5.228	15.55	0.002	4.98
Normal load (B)	2	4.361	4.361	2.181	6.49	0.021	2.08
Filler content (C)	2	125.498	125.498	62.749	186.62	0.000	59.77
A x B	4	1.533	1.533	0.383	1.14	0.404	0.73
A x C	4	57.236	57.236	14.309	42.56	0.000	27.26
B x C	4	8.180	8.180	2.045	6.08	0.015	3.90
Error	8	2.690	2.690	0.336			1.28
Total	26	209.954					100

DOF: Degrees of Freedom; Seq SS: Sequential Sum of Squares; Adj SS: Adjusted Sum of Squares; Adj MS: Adjusted Mean Squares; P: Percentage of Contribution.

The main and interaction effect plots aid to visualize the impact of each factor and its combination on output performance and recognize which factors are most influential. However, a statistical hypotheses test is needed in order to determine if any of these effects are significant. Analysis of variance (ANOVA), which consists of simultaneous hypothesis tests to find out if any of the effects are significant, is performed on the output data.

### 3.3. Analysis of Variance (ANOVA)

Table 4 indicates ANOVA table for friction coefficient of test samples. The last column in Table 4 shows the percentage of contribution of each parameter and their interactions. It can be observed that filler content ( $P = 16.36\%$ ), sliding velocity ( $P = 15.03\%$ ) and normal load ( $P = 12.49\%$ ) are the factors that control frictional behavior of test samples. The interaction between the velocity and filler content ( $P = 21.99\%$ ) is the predominant interaction model

term, and other interaction models are comparatively less significant, and the error contribution in the ANOVA for friction coefficient is 18.25%. The error in the Table 4 is considerable and this kind of errors is common during the statistical analysis of friction phenomena in case of composites. It is clear that sliding velocity and filler content as individual factors and also their interactions are the predominant factors that control the friction coefficient of the test samples.

Table 5 indicates ANOVA table for specific wear rate of test samples. From the table one can observe that the filler content ( $P = 59.77\%$ ), the sliding velocity ( $P = 4.98\%$ ), and the normal load ( $P = 2.08\%$ ) are the controlling factors on the wear of the composites. The interaction between velocity and filler content ( $P = 27.26\%$ ) is found to be the significant interaction model terms. The other interactions are found to be less significant and the error contribution in the ANOVA for wear rate is only 1.28%.

## 4. Conclusions

The present work includes details of extensive study on tribological performance of metal particulate filled epoxy composites. Following are the important observations from the study.

1. The addition of recycled cast iron powder to epoxy has considerably exaggerated the properties of epoxy polymer. Density and hardness of epoxy was found to increase appreciably with the addition of metal filler. It was also observed that filler content greatly influenced the friction and wear behavior of epoxy polymer under dry sliding conditions.
2. ANOVA results indicated that metal filler content is the major contributing factor controlling the friction and wear performance of thermoset epoxy.

From the full factorial analysis, it can be concluded that the metal fillers such as recycled cast iron powders can be used as a tribological additive to thermoset polymers such as epoxy to produce low cost composites.

---

## REFERENCES

- [1] K. Friedrich, Z. Zhang and P. Klein, "Wear of polymer composites", in *Wear – Mechanisms, Materials and Practice* (Editor G.W. Stachowiak), John Wiley and Sons, Ltd, West Sussex, England, 2006, 269-290.
- [2] R.N. Rother, *Particulate filled polymer composites*, Rapra Technology Ltd., Shawbury, United Kingdom, 2nd Edition, 2003.
- [3] F. Bouzat, G. Darsy, S. Foucaud and R. Lucas, 2016, Group 4 Metal-containing polymers: An overview, *Polymer Reviews* 56(2), 187-224.
- [4] A. Qureshi, A. Mergen, M.S. Eroglu, N. L. Singh and A. Gulluoglu, 2008, Dielectric properties of polymer composites filled with different metals, *Journal of Macromolecular Science Part A* 45(6), 462-469.
- [5] P.L. Teh, H.T. Ng and C.K. Yeoh, 2011, Recycled copper as the conductive filler in polyester composites, *Malaysian Polymer Journal* 6(1), 98-108.
- [6] M.T. Tomczak, R. Steller, J. Ziąja, G. Szafran and P. Szymczyk, 2014, Preparation and properties of polymer composites filled with low melting metal alloys, *Polymer-Plastics Technology and Engineering* 53(5), 481-487.
- [7] B. Martorana, G. Carotenuto, D. Pullini, K. Zvezdin, G. La Peruta, P. Perlo and L. Nicolais, 2006, Preparation of plastic ferromagnetic composite materials for magnetic encoders, *Sensors and Actuators A* 129, 176-179.
- [8] J. He, L. Zhang, C. Li, B. Yan and R. Tang, 2013, The effects of copper and polytetrafluoroethylene (PTFE) on thermal conductivity and tribological behavior of polyoxymethylene (POM) composites, *Journal of Macromolecular Science, Part B: Physics* 50(10), 2023-2033.
- [9] K. Ji, Y. Xia and Z. Dai, 2013, Different foamed metal-reinforced composites: Tribological behavior and temperature field simulation, *Tribology Transactions* 56(4), 615-622.
- [10] M. Mohamed, A. Maghraby, M. A. Latif, H. Farag and K. Kalaitzidou, 2013, Fe-Ni alloy/polyamide 6 nanocomposites: effect of nanocrystalline metal particles on the mechanical and physical properties of the polymer, *Journal of Polymer Research* 20, 137-147.
- [11] M.S. Bhagyashekar and R.M.V.G.K. Rao, 2010, Characterization of mechanical behavior of metallic and non-metallic particulate filled epoxy matrix composites, *Journal of Reinforced Plastics and Composites* 29(1), 30-42.
- [12] W. Brostow, A. Buchman, E. Buchman and O.O. Mejia, 2008, Microhybrids of metal powder incorporated in polymeric matrices: friction, mechanical behavior, and microstructure, *Polymer Engineering and Science* 1977-1981.
- [13] M. Kumar and J. Bijwe, 2010, NAO friction materials with various metal powders: Tribological evaluation on full-scale inertia dynamometer, *Wear* 269, 826-837.
- [14] K. Ji, Y. Xia, H. Wang and Z. Dai, 2012, Foamed-metal reinforced material: Tribological behaviours of foamed-copper filled with polytetrafluoroethylene and graphite, *Proceedings of the Institution of Mechanical Engineers, Part J: Journal of Engineering Tribology* 226, 123-137.
- [15] A. Rempp, A. Killinger, and R. Gadow, 2012, New approach to ceramic/metal-polymer multilayered coatings for high performance dry sliding applications, *Journal of Thermal Spray Technology* 21 (3-4), 659-667.
- [16] R.V. Kurahatti, A.O. Suredranathan, S.A. Kori, A.V.R. Kumar, B. Mordina and D.G. Mallapur, 2011, Friction and dry sliding wear behaviour of Ni filled epoxy nanocomposite, *Tribology - Materials, Surfaces & Interfaces* 5(2), 49-52.
- [17] S. Shang, G. Song, X. Chu, L. Zhang and F. Chang, 2014, AC and DC behavior of finger-sensing metal/polymer composites at various pressures, *Composites Science and Technology* 97, 115-120.
- [18] S. B Lee, J.Y. Choi, W.W. Park, J.H. Jeon, S.O. Won, J.Y. Byun, S.H. Lim, and S.H. Han, 2010, A study of TiN-coated metal-on-polymer bearing materials for hip prosthesis, *Metals and Materials International* 16(4), 679-686.
- [19] V. Zaporozhchenko, T. Strunskus, K. Behnke, C.V. Bechtolsheim, M. Kiene and F. Faupel, 2000, Metal/polymer interfaces with designed morphologies, *Journal of Adhesion Science and Technology* 14(3), 467-490.
- [20] M. Sudheer, R. Prabhu, K. Raju, T. Bhat 2012, Optimization of dry sliding wear performance of ceramic whisker filled epoxy composites using Taguchi approach, *Advances in Tribology* 2012, 431903, 1-9.
- [21] M. Sudheer, R. Prabhu, K. Raju, T. Bhat, 2013, Modeling and analysis for wear performance in dry sliding of Epoxy/Glass/PTW composites using full factorial techniques, *ISRN Tribology* 2013, 624813, 1-11.
- [22] S. Bahadur, 2000, The development of transfer layers and their role in polymer tribology, *Wear* 245 (1-2), 92-99.