

Effect of Accelerated Chemical Degradation on the Surface Roughness Parameters and Morphology of Fuel Cell Membranes

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Abstract Nafion[®] membranes are proton conducting membranes that are widely used in fuel cells. This study investigates the surface roughness evolution and morphology change in the Nafion[®] 212 membrane (N212) subjected to two types of artificial degradation. Although some previous investigations have clearly observed the difference in morphological changes of the membrane subjected to different accelerated degradation techniques, very scant information available on the roughness parameters of the membrane. Given the rough surface nature of the catalyst layer (CL), information obtained from the present investigation can be helpful in understanding the interfacial stability of the membrane electrode assembly (MEA). We distinguish and compare the morphological changes in the membrane with the published observations and note that different accelerated degradation mechanisms lead to distinguished changes in the N212 morphology. Two chemical degradation techniques adopted here are – Ion exchange method and Solution method. Tapping mode - AFM (TM-AFM) and SEM is used in investigating the roughness parameters and surface morphology of the fresh as well as degraded N212.

Keywords Accelerated degradation, Surface roughness, Solution method, Ion-exchange method, Nafion[®] membrane, Tapping mode – AFM, Surface morphology

1. Introduction

Durability, stability, and reliability requirement of the PEM fuel cell layers are demanding innovative researches on the new materials, mostly MEA. MEA draws considerable interest among researchers, as it is vulnerable for damage and degradation under fuel cell working conditions [1-3]. Therefore, analyzing and understanding the root causes of performance decay or electro-chemical or mechanical degradation will give much justice in finding answers in terms of alternative materials as well as ideal stack design. Low temperature membranes used in PEM fuel cells are susceptible for electro-chemical or mechanical degradation and is generally unavoidable. And under fuel cell operating conditions membrane is subjected to severe durability issues that are compounded by mechanical and hygrothermal stresses, cracking and interfacial delaminations and are realized in the form of fuel cross over and water management problems. Hence, to shed a light on the fundamentals of membrane degradation,

multi-disciplinary approaches and breakthroughs are needed and in the process, recently, many researchers have proposed various mechanisms that are mainly related to chemical [4-13] and mechanical [14-21] degradation.

It has long been known that the chemical degradation lead to structural (chemical) as well as morphological changes in the membrane. Chemical degradation of membrane is understood to be due to hydroxyl radicals attack on the carboxylic end groups of nafion membrane. Literature has witnessed in following the artificial degradation procedures that induce same effect like what happens under real situation, but in a shorter amount of time, and is termed as accelerated degradation. There are two major accelerated chemical degradation methods, namely, solution method and ion exchange method. Although two of these methods claimed to induce same chemical changes, distinguished morphological features in the membrane can be observed. On a most important note, morphological changes in the degraded membrane not only differ for degradation mechanisms but also membrane type. For example, Kundu et al. [11] performed two of the above mentioned degradation methods on Nafion[®] 112 membrane (N112) and they observed significant differences in the degradation methods in terms of membrane's morphological structure. Further, Fernandes and Ticianelli

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[12] performed ion exchange degradation on Nafion 112 and Nafion 212 and reported that N212 was subjected to severe morphological changes as opposed to N112. Interestingly, observable morphological changes on N212 induced by ion exchange method [12] were similar to the changes on N112 induced by solution method [11].

Apart from the degradation methods on different membrane types, morphological changes in the degraded membrane require more explanations in terms of their influence on damage initiation and propagation in the membrane as well as near interfaces. Researchers have investigated nafion membrane in different forms and under different conditions (dry or humid) using AFM in order to recognize and differentiate the hydrophilic and hydrophobic domains [22-29]. Although several experimental results focused on nano-structural changes in the membrane, evolution of roughness parameters in the degraded membranes are not clear. This is because, artificial degradation, in general, leads to bubble or hole or damage evolution in the membrane surface which makes inadequate for AFM to probe under large scan dimension, that means, scanning ability entirely depends on how severe the membrane is degraded and again it depends on the membrane types and the degradation methods. There can be two simple observations drawn from literature outcomes. High-resolution AFM scan (refers to nm scan dimension) is generally used to observe the nano-structural changes in the membrane. While low resolution AFM scan (refers to μm scan dimension) of the membrane can be used to estimate the tribological parameters (here roughness) that can effectively be used to explain the effect of membrane degradation on the interface characteristics in future studies.

2. Experimental

We perform chemical degradation technique using two of the generally known methods on N212 membrane in order to understand their effect on surface morphologies.

2.1. Solution Method

This method is similar to the method proposed by Kundu et al. [11] and Healy et al. [13]. The solution method used 30% H_2O_2 mixed with $\text{FeCl}_2 \cdot 4\text{H}_2\text{O}$ to produce a 16 mg/L solution of Fe^{2+} ions. This solution (40 mL) was placed in a closed vial containing Nafion samples. The Nafion and solution were kept in 80°C oven for 24 h or 48 h or 72 h and the solution of peroxide and iron was replaced by fresh solution at every 12 h. After these times, the samples were removed from the solution, rinsed and saved for AFM or SEM investigation.

2.2. Ion Exchange Method

This method is similar to the method proposed by Fernandes and E. A. Ticianelli [12] and Kinumoto et al. [30]. Samples of Nafion 212 were soaked in a saturated solution of $\text{FeCl}_2 \cdot 4\text{H}_2\text{O}$ for 24 h. The samples were then

rinsed with highly purified water for at least 1 h. Next, they were left in vials to which 40 mL of hydrogen peroxide solution was added, for 24 h or 48 h or 72 h at a temperature of 80°C . After these times, the samples were removed from the solution, rinsed and then conditioned in 1 M H_2SO_4 to remove any residual iron and then the membrane was returned into the H^+ form.

2.3. Tapping Mode AFM

Degraded membrane samples were subjected to TM-AFM (TM-AFM has an edge over contact AFM in that the pressure applied by the former is much lower and hence sample surface is less perturbed by the tip.) using Nanoscope IV Multimode scanning probe. Membrane samples (about $5 \times 5 \text{ mm}$) are mounted on microscope slides using epoxy, such that the glue does not seep out from underneath the membrane film. For the reasons mentioned in section 1, scan size dimension was chosen to be around $4 \times 4 \mu\text{m}$. Roughness parameters investigated are defined as follows:

- (a) Mean roughness (R_a): It is defined as the average absolute deviation of the roughness irregularities from the mean line over one sampling length L as shown in Fig. 1(a). It is also referred as Centerline average (CLA). This parameter is insensitive to small changes in profile although it is easy to measure [31]. The mathematical definition of R_a is as follows:

$$R_a = (1/L) \int_0^L |y| dx \quad (1)$$

- (b) Root mean square (RMS) roughness (R_{rms}): It represents the standard deviation of the distribution of the surface heights. This parameter is more sensitive to large deviation from the mean line as opposed to R_a . The mathematical definition of R_{rms} is as follows:

$$R_{rms} = \sqrt{(1/L) \int_0^L |y|^2 dx} \quad (2)$$

- (c) Maximum peak height (R_p): This represents the distance between peaks and valleys over a sampling length in a roughness profile as stated in Fig. 1(b).
 (d) Mean asperity radius (r_m): This parameter is calculated by calculating the radius of curvature for each peak along the profile, then averaging it. Mathematical definition of this is as follows [31]:

$$r_m = \frac{(2y_i - y_{i-1} + y_{i+1})}{l^2} \quad (3)$$

Ten point mean roughness (R_z): This parameter is more sensitive to occasional high peaks or deep valleys than R_a . It is defined as the difference in height between the average of the five highest peaks and five lowest valleys along the sampling length as shown in Fig. 1(c). Simplified expression

for this is as follows:

$$R_z = \frac{\left(\sum_{i=1}^{i=5} |y_{p_i}| + \sum_{j=1}^{j=5} |y_{v_j}| \right)}{5} \quad (4)$$

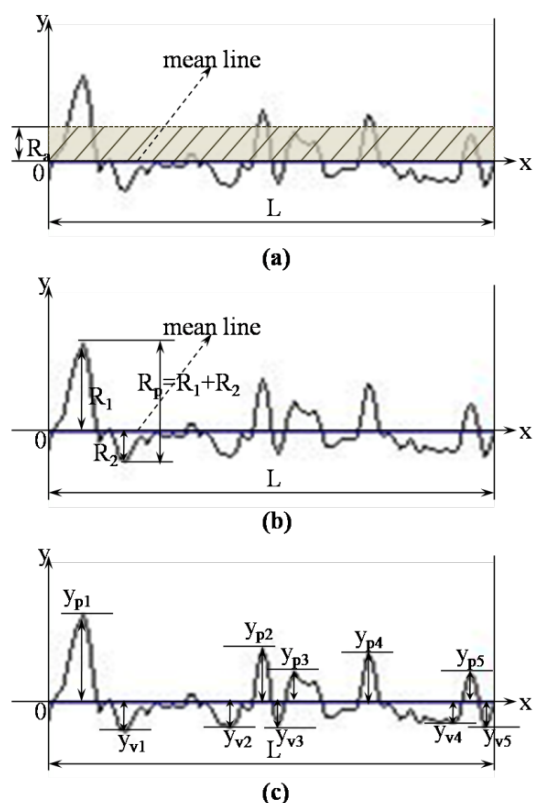


Figure 1. (a) Definition of Mean roughness (Ra). (b) Definition of Maximum peak height (Rp). (c) Definition of Ten-point mean roughness (Rz)

3. Results and Discussion

3.1. TM-AFM

Fig. 2(a) shows the AFM image of fresh N212 membrane along with the sectional line analysis. On the right side of Fig. 2(a), small variations in the surface heights can be observed which corresponds to the actual surface morphology of the membrane characterized by nodular aggregates. For comparison purpose, images are taken at same scan dimension ($4 \times 4 \mu\text{m}$), although the nanostructure of membrane can be explored under high resolution (e.g. under $1 \times 1 \mu\text{m}$). Contrary to this observation, Fig. 2(b) shows the surface image of degraded membrane (solution method for 24 h) with higher density of bright spots corresponding to the distribution density of asperity heights. Sectional analysis of the degraded sample (on the right side) indicates a remarkable increase in the roughness parameters as opposed to fresh membrane with RMS roughness value of 5.14 nm. Roughness parameters described in section 2.3 are estimated in Table 1 for fresh as well as degraded

membranes (degraded by solution method). Further, degradation using solution method of membrane for 72 h results in an increased level of roughness with a RMS value 12.3 nm as plotted in Fig. 2(c). Further, 3-dimensional scan of fresh membrane as represented in Fig. 2(d) roughly shows the spherically shaped nodular aggregates, which is characteristic of molecular structure of the ionomeric materials [23]. (Although nodular aggregates claimed to induce surface roughness as investigated by Lehmani et al. [23], they are negligible at least in reference to the CL/membrane interface toughness instability). Since, many researchers have already made significant progress on this observation; it is not repeated here. Our interest is on Fig. 2(e) that shows the 3-dimensional evolution and distribution of asperity heights which covers the basic structure of the membrane and hence it is no more possible to observe nodular structure. This image corresponds to the 2-D surface scan as shown in Fig. 2(b). As the degradation time increases roughness also increases and is again evident from Fig. 2(f).

Further, it is noted from Table 1 that there is a direct correlation between increase in the roughness parameters to the exposure time except for mean asperity radius r_m . Although mean roughness for 72 h of degradation is higher than the 24 h of degradation, peak radius tends to decrease while increasing the chances of peak wear out or damage accumulation near interfaces.

It was not possible to access the surface roughness parameters of the membrane degraded under ion exchange method and reasons for this will be discussed in the following section.

3.2. SEM

Fig. 3(a) shows the SEM surface image of the membrane degraded by ion exchange method. Bubble formation and the circumferential tears around the bubbles are observed. It is noted that this observation on N212 membrane is similar to the findings of Fernandes and Ticianelli [12] on N212 (ion exchange degradation) and Kundu et al. [11] on N112 (solution method of degradation). However, magnified image of Fig. 3(a) shows the nodular aggregates separated by a micro-crack as shown in Fig. 3(b). Further, as the exposure time increases, small bubbles transform into larger ones followed by tears as well as tiny fractures as shown in Fig. 3(c) and (d). This is also marked by a bulging of a surface that can roughly be observed. This bulging of surface comes from the membrane bursting from the center, which is characterized by a centerline crack in the SEM cross section image as shown in Fig. 3(e).

All these discussed observations are found to make a negative impact in accessing the roughness parameters by TM-AFM, nevertheless it highly indicates that damage induced by ion exchange method on N212 is severe than the solution method of degradation. This is further clarified in Fig. 3(f), where the membrane surface is characterized by very small particles that appear to have loosely distributed

and this corresponds to high-density peaks explored by TM-AFM study (Figs. 2(e) and (f)). It is further noted that the magnification of Fig. 3(b) and Fig. 3(f) is same but surface appears to be different, indicating that the different degradation methods induces distinguished morphological results.

Thus, revelation of damage evolution in a membrane in relation to the surface roughness is better understood by solution method of degradation on N212, while the mechanical damage propagation or mitigation in the membrane can be estimated by ion exchange method of degradation on N212. Moreover, such high-density evolution of nano-sized asperity peaks in the chemically

degraded membrane are highly vulnerable to plastic deformation, which can trigger a damage accumulation and then propagation, which can then become catastrophic for interfacial toughness between the membrane and CL. On the other hand, observable valleys in the degraded membranes may play a crucial role in mass transport loss in the membrane. This is because, degradation of catalyst layer leads to the disintegration of its constituents, which subsequently settles into valleys of the membrane leading to valley clogging. This might become obstacle in smooth electro-chemical performance of membrane as it might affect the water or proton flux rates.

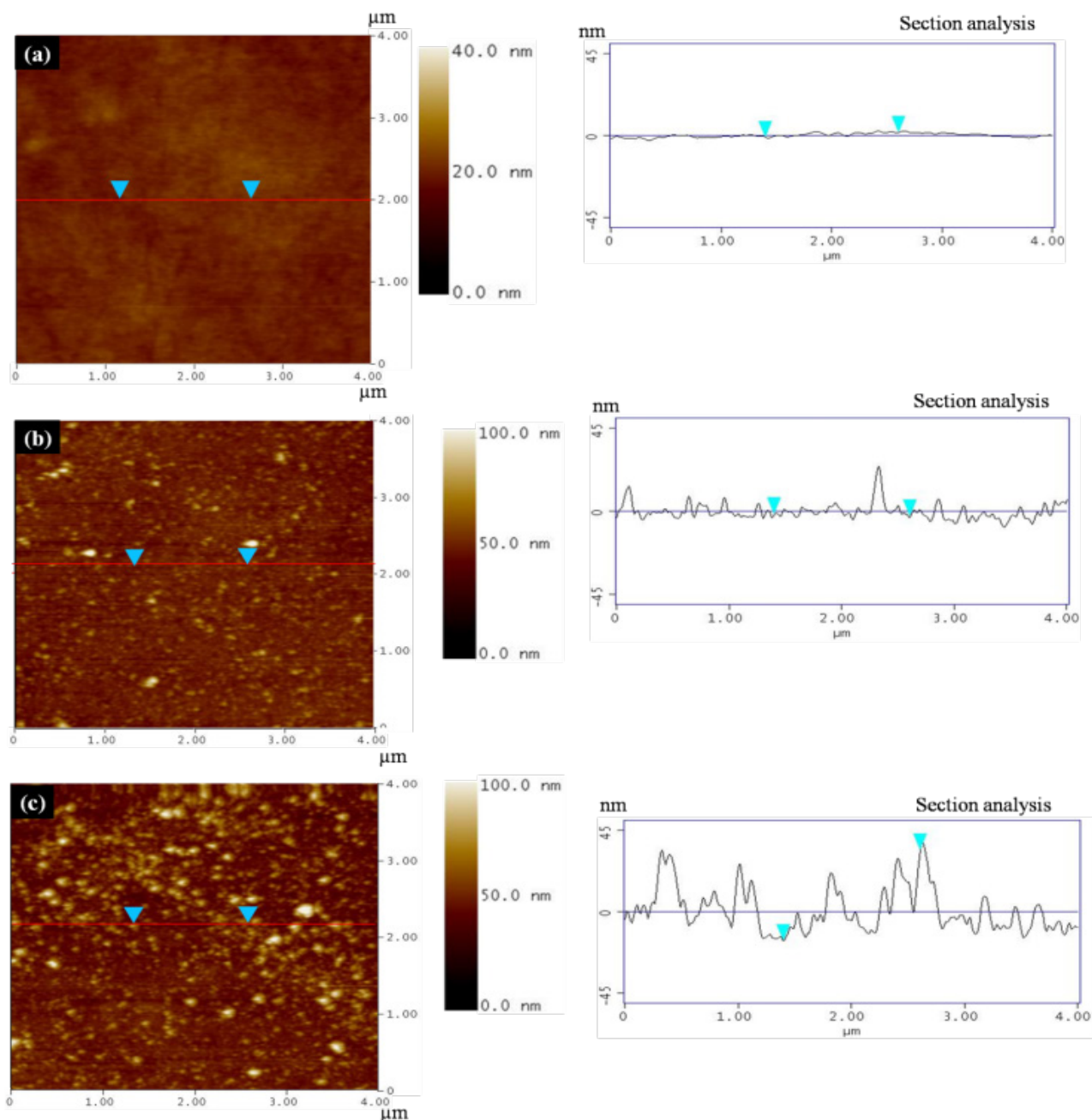
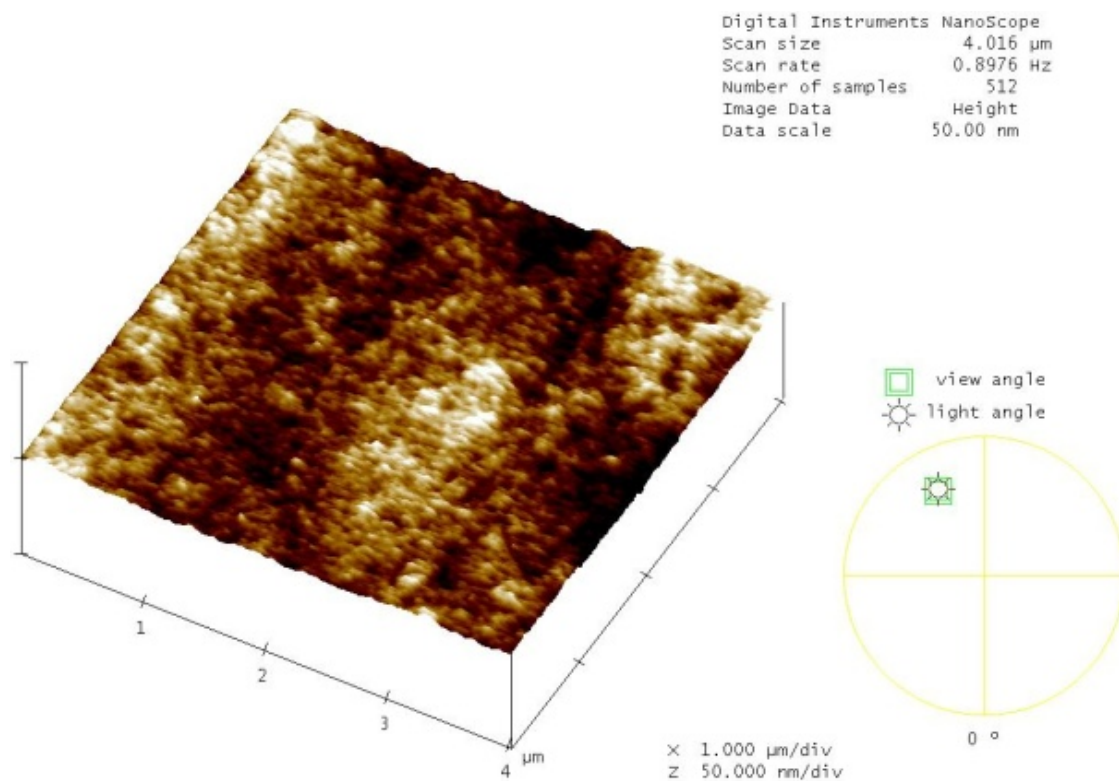
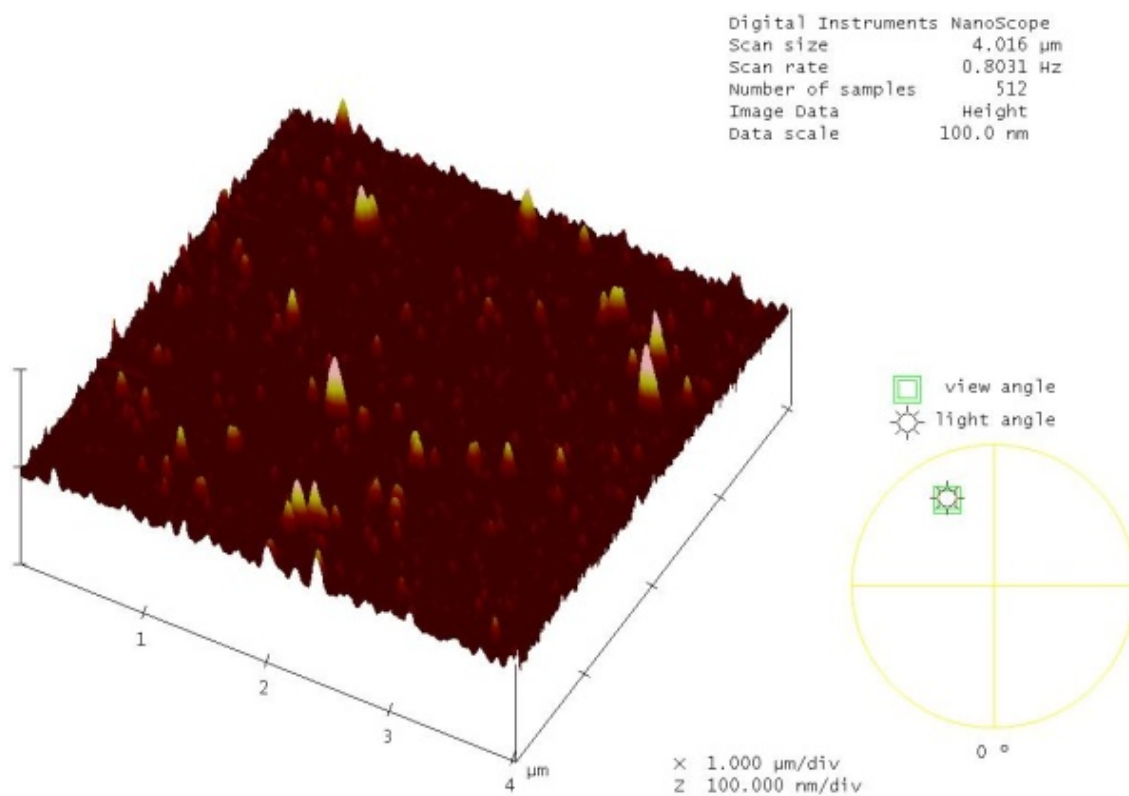


Figure 2. TM-AFM sectional analysis on (a) Fresh N212 membrane. (b) Degraded membrane using solution method (exposure time – 24 h). (c) Degraded membrane using solution method (exposure time – 72 h)



(d)



(e)

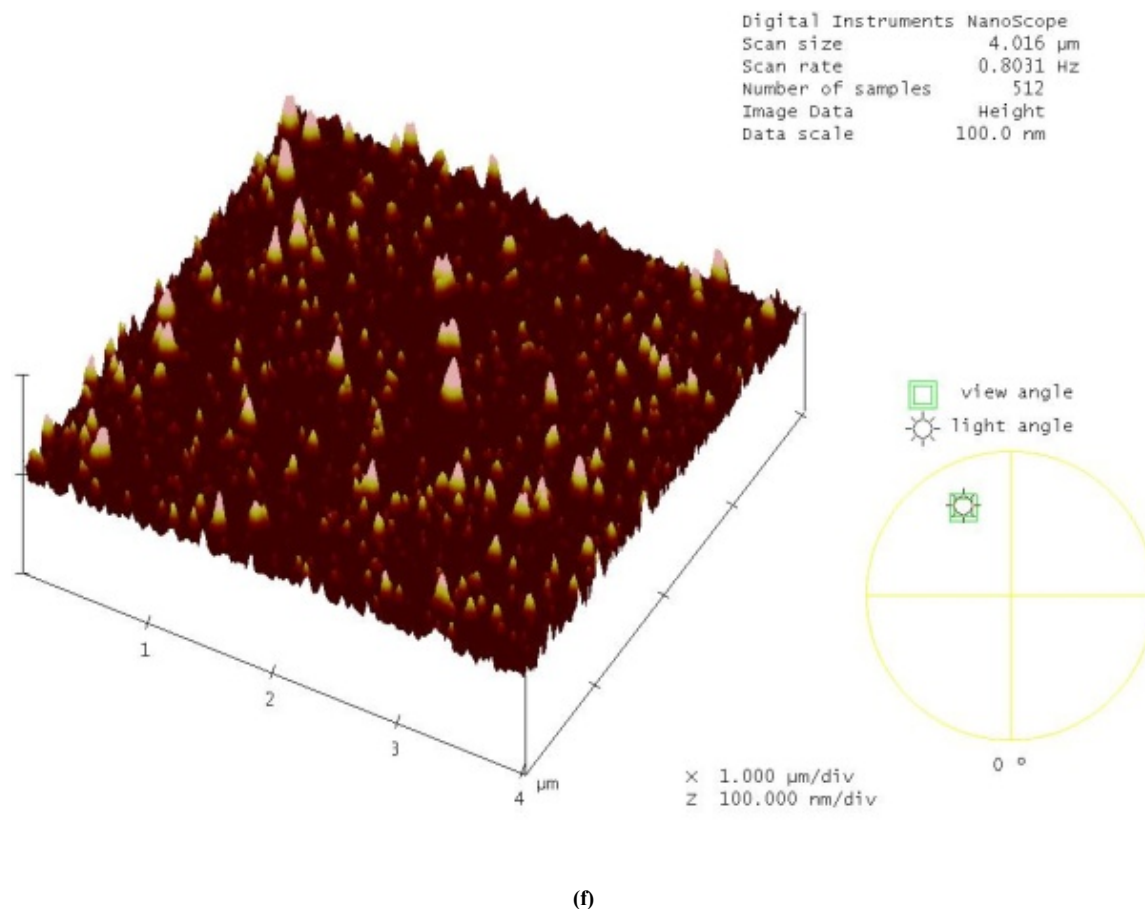


Figure 2. TM-AFM 3-D scan of (d) Fresh N212 membrane. (e) Degraded membrane using solution method (exposure time – 24 h). (f) Degraded membrane using solution method (exposure time – 72 h)

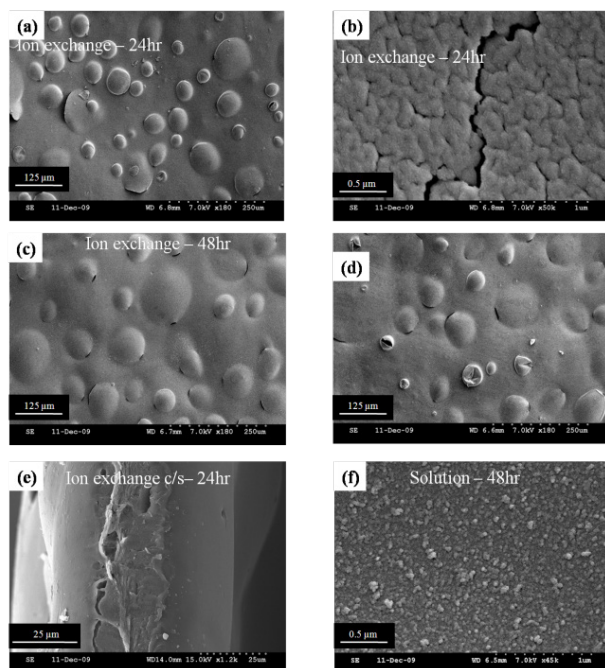


Figure 3. SEM micrographs of N212 for (a) ion exchange degradation – 24 h. (b) enlarged image of (a) showing a micro-crack. (c) ion exchange degradation – 48 h. (d) ion exchange degradation – 72 h. (e) cross section of degraded membrane induced by ion exchange method – 48 h. (f) solution method of degradation – 24 h

4. Conclusions

This study investigates the surface roughness evolution and surface morphology of N212 membrane subjected to two types of artificial degradation techniques. Interestingly, solution method and ion exchange method of degradation results in distinguished surface morphology of the membrane. The membrane samples of N212 degraded by solution method is found to be useful in extracting the surface roughness parameters, while the samples degraded by ion exchange method can be useful in understanding the damage evolution and propagation in the membrane. This also means that solution method of degradation produces less severe damage than the ion exchange method on N212 and this contradicts the previous outcomes on N112 membranes [11]. Evolution of surface roughness parameters in the degraded membrane obtained from solution method marked by the evolution of asperity peaks and valleys can be used in predicting the interfacial toughness of membrane/CL interface, in the future study.

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REFERENCES

- [1] K.K. Poornesh, C.D. Cho, G.B. Lee, Y.S. Tak, Gradation of mechanical properties in gas diffusion electrode. Part 1: Influence of nano-scale heterogeneity in catalyst layer on interfacial strength between catalyst layer and membrane. *Journal of power sources* 2010, 195, 2709-2717.
- [2] K.K. Poornesh, C.D. Cho, G.B. Lee, Y.S. Tak, Effect of gas-diffusion electrode material heterogeneity on the structural integrity of polymer electrolyte fuel cell. *Energy* 2010, 35, 5241-5249.
- [3] K.K. Poornesh, C.D. Cho, Poroelastic PEM fuel cell catalyst layer and its implication in predicting the effect of mechanical load on flow and transport properties. *International Journal of hydrogen energy* 2011, 36, 3623-3634.
- [4] V. O. Mittal, H. R. Kunz, J. M. Fenton, Membrane degradation mechanisms in PEMFCs. *Journal of the Electrochemical Society* 2007, 154, B652-B656.
- [5] V. A. Sethuraman, J. W. Weidner, A. T. Haug, L.V. Protsailo, Durability of perfluorosulfonic acid and hydrocarbon membranes: Effect of humidity and temperature. *Journal of The Electrochemical Society* 2008, 155, B119-B124.
- [6] N. Ramaswamy, N. Hakim, S. Mukerjee, Degradation mechanism study of perfluorinated proton exchange membrane under fuel cell operating conditions. *Electrochimica Acta* 2008, 53, 3279-3295.
- [7] V. A. Sethuraman, J. W. Weidner, A. T. Haug, S. Motupally, L.V. Protsailo, Hydrogen peroxide formation rates in a PEMFC anode and cathode - Effect of humidity and temperature. *Journal of The Electrochemical Society* 2008, 155, B50-B57.
- [8] M. Inaba, T. Kinumoto, M. Kiriake, R. Umebayashi, A. Tasaka, Z. Ogumi, Gas crossover and membrane degradation in polymer electrolyte fuel cells. *Electrochimica Acta* 2006, 51, 5746-5753.
- [9] S. Zhang, X. Yuan, H. Wang, W. Me'rida, H. Zhu, J. Shen, S. Wu, J. Zhang, A review of accelerated stress tests of MEA durability in PEM fuel cells. *International Journal of hydrogen energy* 2009, 34, 388 - 404.
- [10] S. Kundu, M.W. Fowler, L.C. Simon, S. Grot, Morphological features (defects) in fuel cell membrane electrode assemblies. *Journal of Power Sources* 2006, 157, 650-656.
- [11] S. Kundu, M.W. Fowler, L.C. Simon, S. Grot, Comparison of two accelerated Nafion™ degradation experiments. *Polymer Degradation and Stability* 2008, 93, 214-224.
- [12] A. C. Fernandes, E. A. Ticianelli, A performance and degradation study of Nafion 212 membrane for proton exchange membrane fuel cells. *Journal of Power Sources* 2009, 193, 547-554.
- [13] J. Healy, C. Hayden, T. Xie, K. Olson, R. Waldo, M. Brundage, H. Gasteiger, J. Abbott, Aspects of chemical degradation of PFSA ionomers used in PEM fuel cells. *Fuel Cell* 2005, 5, 302-308.
- [14] A. Kusoglu, A.M. Karlsson, M.H. Santare, S. Cleghorn, W.B. Johnson, Mechanical Behavior of Fuel Cell Membranes under Humidity Cycles and Effect of Swelling Anisotropy on the Fatigue Stresses. *Journal of Power Sources* 2007, 170, 345-358.
- [15] D. Bogachev, M. Gueguen, J. C. Grandidier, S. Martemianov, Stress and plastic deformation of MEA in fuel cells: Stresses generated during cell assembly. *International Journal of hydrogen energy* 2008, 33, 5703-5717.
- [16] K.K. Poornesh, C.D. Cho, G.B. Lee, Y.S. Tak, Gradation of mechanical properties in gas-diffusion electrode. Part 2: Heterogeneous carbon fiber and damage evolution in cell layers. *Journal of Power Sources* 2010, 195, 2718-2730.
- [17] J. Xie, III Wayne, T.A. Zawodzinski, P. Atanassov, R.L. Borup, Durability of PEFCs at High Humidity Conditions. *Journal of the Electrochemical Society* 2005, 152, A104-A113.
- [18] E. Endoh, S. Terazono, H. Widjaja, Y. Takimoto, Degradation study of MEA for PEMFCs under low humidity conditions. *Electrochem. Solid-State Letters* 2004, 7, A209-A211.
- [19] M. Luo, C. Huang, W. Liu, Z. Luo, M. Pan, Degradation behaviors of polymer electrolyte membrane fuel cell under freeze/thaw cycles. *International Journal of hydrogen energy* 2010, 35, 2986-2993.
- [20] R.C. McDonald, C.K. Mittelsteadt, E.L. Thompson, Effects of Deep Temperature Cycling on Nafion® 112 Membranes and Membrane Electrode Assemblies. *Fuel cells* 2004, 4, 208 - 213.
- [21] A. Pozio, R.F. Silva, M.D. Francesco, L. Giorgi, Nafion degradation in PEFCs from end plate iron contamination. *Electrochimica Acta* 2003, 48, 1543-1549.
- [22] M. Chomakova-Haefke, R. Nyffenegger, E. Schmidt, Structure reorganization in polymer films of nafion due to swelling studied by scanning force microscopy. *Applied Physics A* 1994, 59, 151-153.
- [23] A. Lehmani, S. Durand-Vidal, P. J. Turq, Surface morphology of Nafion 117 membrane by tapping mode atomic force microscope. *Applied Polymer Science* 1998, 68, 503-508.
- [24] P. J. James, T. J. McMaster, J. M. Newton, M. J. Miles, In situ rehydration of perfluorosulphonate ion-exchange membrane studied by AFM. *Polymer* 2000, 41, 4223-4231.
- [25] P. J. James, J. A. Elliott, T. J. McMaster, J. M. Newton, A. M. S. Elliott, S. Hanna, M. Miles, J. Hydration of Nafion (R) studied by AFM and X-ray scattering. *Journal of Materials Science* 2000, 35, 5111-5119.
- [26] R. S. McLean, M. Doyle, B. B. Sauer, High-resolution imaging of ionic domains and crystal morphology in ionomers using AFM techniques *Macromolecules* 2000, 33, 6541-6550.
- [27] P. J. James, M. Antognozzi, J. Tamayo, T. J. McMaster, J. M. Newton, M. J. Miles, Interpretation of contrast in tapping mode AFM and shear force microscopy. A study of nafion. *Langmuir* 2001, 17, 349-360.
- [28] A. M. Affoune, A. Yamada, M. Umeda, Surface observation of solvent-impregnated Nafion membrane with atomic force microscopy *Langmuir* 2004, 20, 6965-6968.

- [29] K. A. Friedrich, M. Schulze, R. Hiesgen, I. Wehl, X.-Z. Yuan, H. Wang, Nanoscale Investigation of Nafion Membranes after Artificial Degradation. ECS transactions 2009, 25, 395-403.
- [30] T. Kinumoto, M. Inaba, Y. Nakayama, K. Ogata, R. Umebayashi, A. Tasaka, Y. Iriyama, T. Abe,; Z. Ogumi, Durability of perfluorinated ionomer membrane against hydrogen peroxide. Journal of Power Sources 2006, 158, 1222-1228.
- [31] E. S. Gadelmawla, M. M. Koura, T. M. A. Maksoud, I. M. Elewa, H. H. Soliman, Roughness Parameters. Journal of Materials Processing Technology 2002, 123 (1) () 133-145.